

INSTRUCTIONS

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FOR BOILER FEEDPUMP TURBINES 357513TC300

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ELECTRO HYDRAULIC CONTROL FOR BOILER FEEDPUMP TURBINES 357513TC300

INTRODUCTION

The electronic portion of an Electrohydraulic Control system for a boiler feedpump turbine drive is described in these instructions.

Any adjustment or maintenance of this equipment should be performed either by qualified turbine personnel or supervised by such personnel.

Drawing 44C300679 is a block diagram of a typical unit and is referred to later. This equipment is an electronic speed governor whose speed set point can be varied by an automatic boiler controller or by an operator from a remote control unit. Electronic redundancy and mechanical overspeed trip are used to provide a high degree of reliability and safety.

A block diagram, elementary diagram, and alignment diagram for a particular unit are included in these instructions. Since both the number and arrangement of auxiliary components vary with particular application, it is necessary to refer to the drawings furnished with each equipment to determine the correct connections and auxiliary components furnished in each instance.

RECEIVING, HANDLING AND STORAGE

RECEIVING AND HANDLING

Immediately upon receipt, the equipment should be carefully unpacked to avoid damaging the apparatus. Particular care should be exercised to prevent small parts being mislaid or thrown away in the packing material.

As soon as the equipment is unpacked it should be examined for any damage that might have been sustained in transit. If injury or rough handling is evident, a damage claim shall be filed immediately with the transportation company and the nearest General Electric Sales Office should be notified promptly.

STORAGE

If the equipment is not to be used as soon as it is unpacked, it should be stored in a clean dry place and protected from accidental damage. Particular care should be exercised to avoid storing the equipment in locations where construction work is in progress.

DESCRIPTION

The speed control loop will be described first. Starting outside the electronic control unit on the right hand side of block diagram 44C300679 an electrohydraulic valve receives a low power electrical

signal from the electronic unit and controls the flow of oil to a double acting hydraulic cylinder which positions the turbine steam control valve. Turbine speed is sensed by two magnetic sensors mounted near the periphery of a shaft driven gear. Pulses whose frequency is directly proportional to turbine speed are generated as each gear tooth passes a sensor. Primary and secondary speed channels in the electronic control produce a DC voltage proportional to the frequency of the sensor outputs. Outputs of the two speed channels are fed into high valve gate number, one which rejects the lower of the two speed signals and passes on the higher valued signal. This redundancy permits one channel to fail without significantly affecting turbine speed. The secondary channel is adjusted for an output, 1% less than the primary channel. It is therefore uncontrolling, except in case of failure of the primary channel or if a "Backup Amplifier Test" switch in the cabinet is actuated which increases the output of the secondary channel to 1% greater than the primary channel. A test meter in the cabinet can be used to determine the controlling channel.

The speed signal from high valve gate one is summed with the speed set point to obtain a speed error. See the middle of the block diagram. The speed error is passed through a stability compensation and error amplifier, which includes a regulation adjustment to obtain a valve lift demand signal. This is summed with a valve position signal to obtain a valve position error which is passed through the servo amplifier to the servo valve. Increasing the speed set point increases valve lift demand, valve position error, and valve opening. Speed will increase until the rise matches the set point increase.

The valve position signal is obtained from a linear variable differential transformer (LVDT) whose core is positioned by the control valve. Three kilohertz excitation for the LVDT is generated in the electronic cabinet. A demodulator in the cabinet produces a DC signal proportional to the AC output of the LVDT which varies with core position.

The electronic control unit applies a strong close signal to the servo valve in the tripped condition. Before the control can be reset, it must generate a close valve signal from the governor. Relay circuitry also requires that the electrical connectors must be plugged into the servo valve, the LVDT, and the speed sensors before starting. The LVDT signal is biased to close the control valve if the LVDT connector is removed with the turbine running. The servo valve contains a 5% mechanical bias which will close the control valve in the absence of an electrical signal.

SPEED REFERENCE OR SET POINT

Identical motor driven LVDT's are used to generate the manual and automatic speed references. The core position is varied by a two-phase stepping motor which moves in discrete steps and locks in position when not running. Raise and Lower pushbuttons on the operator's manual control panel cause the reference to run from stop to stop in 80 to 90 seconds. Raise Fast and Lower Fast pushbuttons will run the reference from stop to stop in approximately 10 seconds. The automatic speed reference circuits contain interface circuitry for compatibility with a specific boiler controller. The automatic and manual speed references are fed into a low value gate which rejects the higher reference and passes on the lower reference to control turbine speed. A relay operated from this gate indicates which of the two references is controlling.

An overspeed test can be performed after first running both manual and automatic references to the high speed stop. The operator's overspeed test pushbutton is then actuated causing an additional speed reference to be generated which increases linearly with time at approximately 12% speed per minute. This is added to both manual and automatic references. Once the speed ramp starts, a relay energizes a lamp to indicate that a high reference condition exists. If turbine speed rises to 120% of rated, a speed signal will override the ramp generator and prevent further speed increase. Upon release of the Test pushbutton, the reference ramps back to normal at the same rate as it increased.

The control cabinet includes circuitry for driving position indicators from LVDT's mounted on the stop valves, but this circuitry is not a part of the governor.

Two rectifier-inverter-rectifier power supplies provide necessary DC voltages to the electronics. For startup and operating backup power, one supply is fed from 115 volts, 60 Hz, 1 phase. For primary operating power independent of the AC line, power is obtained from a turbine driven 3-phase permanent magnet generator (PMG).

The PMG also drives a frequency to voltage converter for a tachometer and operates speed relays. A 10% speed relay is combined with the output of speed signal high value gate 2 to cause the speed reference to go to zero if the PMG is above 10% speed and neither primary or secondary speed channel is working. Above 60% speed a relay unlocks the alarms on the PMG power supplies. Above 105% speed a relay unlocks the lock out valve in the emergency trip exerciser scheme.

INVERTERS

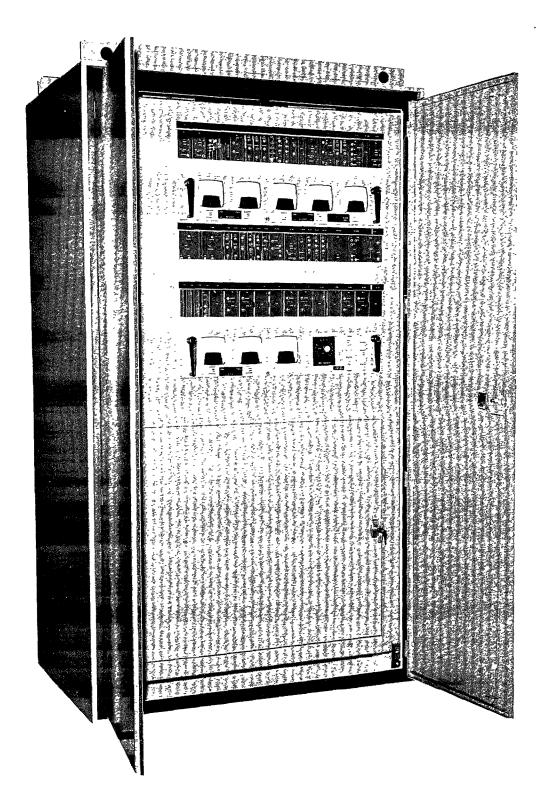
Diagram 44D300970 shows the inverter components. Incoming AC power at C, 1-2 feeds transformer 2T.

The output of 2T is rectified and filtered to obtain an operating DC bus level of 100 to 200 volts. Power elements of the inverter consist of 1-4 SCR thyristors together with commutating reactors, diodes, and capacitors which produce square-wave AC on the primary of transformer 1T. 1T has three secondaries whose outputs are rectified, filtered, and fed through series regulators. Thyristors 1 and 2are operated as a pair such that when either is being fired the other is not fired. Thyristors 3 and 4 are operated similarily. Starting with 1 and 3 conducting and 2 and 4 non-conducting both points B and C are at DC bus level A and no voltage appears across the primary of 1T. 2SCR is then fired placing voltage B on 3-4 of 1X. By transformer action this voltage also appears on 1-2 of 1X which places 1 of 1X at twice voltage A to reverse bias and turn off 1SCR, capacitor 3C quickly discharges through 2 SCR and 1X to zero volts at B. Voltage now appears on 1T primary with C positive with respect to B. This voltage is integrated and when the desired voltsseconds on 1T is obtained 4 SCR is fired. 3 SCR is commulated off, and the voltage at C then goes to zero and the voltage on 1T is again zero. A frequency controlling master flip-flop then fires 1 SCR to raise B to bus level A which reverses the polarity of the voltage previously applied to 1T. Point B is now positive with respect to C. After accumulation of the required volt-seconds. 3 SCR is fired and point C raised to level A which completes one full cycle of the inverter.

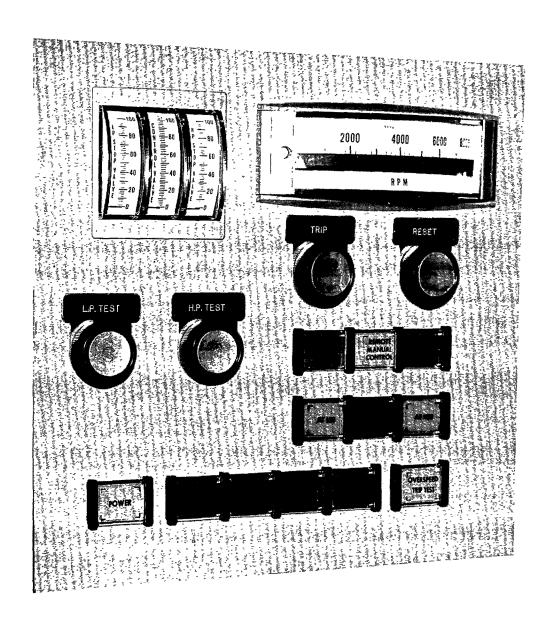
Firing circuits 1-4 FC for the thyristors are shown by dotted blocks just below the bridge circuit and are shown in detail in the lower right corner. A 47 volt bus for the firing circuits is obtained from the DC bus through 2R and 1 ZD. Each firing circuit is a transistorized, transformer coupled blocking oscillator operating at 25 kHz to 100 kHz. A half-wave rectifier on the transformer output winding feeds the associated thyristor gate with pulses at the oscillating frequency. The circuit will oscillate in the absence of a control signal and stop oscillating when a signal is applied.

The inverter control circuitry diagram is shown on the lower portion of diagram 44D300970 from left to right. A 24 volt control bus is obtained from the DC bus through 1R and Zener diode 2 ZD.

The inverter output frequency is approximately 200 Hz is exactly half the frequency of the relaxation oscillator composed of 4C, 4R, 1SUS, and 1X. Capacitor 4C charges through resistor 4R until its voltage equals the break down voltage of silicon unilateral switch 1SUS. When 1SUS breaks down, the voltage drops to a low value placing 4C voltage on 1X and turning on 1Q for approximately 20 microseconds until the discharge of 4C and inductive reversal of voltage on 1X turns off 1Q and 1SUS. Capacitor 4C then begins to charge again. Each conduction pulse of 1Q triggers master flip-flop 1Q-2Q, switching conduction of 1SCR and 2SCR to initiate a half cycle



TYPICAL CABINET
Figure 1
GEK-15019



TYPICAL OPERATORS CONTROL UNIT Figure 2 GEK-15019

of inverter output voltage. The end of each half cycle of output is obtained from switching conduction of 3-4 SCR by slave flip-flop 7Q-8Q.

Regulation of the output volt seconds is obtained from 3D through 8D, 4Q, 5Q, 6Q, 17Q, and associated components. Voltage waveforms for the output, flip-flops, 5-ID diodes, and 4Q, 5Q are shown in Figure 3.

Only during periods of output voltage is 5Q turned off and 8C allowed to charge. The voltage on 8C is the time integral of the current into it, which comes from the DC bus through 16R, 23R, and 1 P.

Transistors 6Q and 17Q trigger on when the capacitor voltage rises above the 6Q base voltage. The discharge of 8C generates a spike on 17 R to trigger slave flip-flop 7Q-8Q ending the half cycle of output voltage.

The remainder of the inverter control components shown to the right of slave flip-flop 7Q-8Q are used to obtain correct start-up of the inverter. When power is applied and voltage begins to build up on the DC bus, it is initially too low to cause conduction of 9Q. With 9Q off, 10Q is on, 12Q off, 13Q on, 14Q off, 15Q on and 16Q on. With 14Q off, its high collector voltage is coupled through 47R and 49R to 2FC and 4FC to inhibit firing of 2 and 4 SCR, letting the voltage on B and C rise with the bus voltage. With 16Q on, it feeds a relatively high current into 8C causing it to reach firing voltage very quickly so that the slave flip-flop remains in the output voltage state for a very short period. As the DC bus continues to rise, it reaches the point where 9Q conducts. This turns off 10Q raising the voltage on the base of 12Q but not enough to cause conduction. Following this, the first flip of the master flip-flop to the 2Q on state is capacitively coupled to 11Q through 11C to momentarily turn it off, allowing its collector to rise and raise the base of 12Q high enough to turn it on and turn off 13Q. The emitter voltage drops and 12Q remains on when the pulse from 11Q disappears. With 13Q off, 14Q is on and 2FC and 4FC are no longer inhibited from firing. 4SCR fires and a short duration output is obtained, quickly ended by the rel-actively high current into 8C triggering the state of the slave flip-flop to the no output voltage condition. With 14Q on 15Q is off and 13C begins to discharge, reducing the current from 16Q into 8C. The time for 8C to reach firing voltage of 6Q-17Q is increased as is the width of the output voltages waveform until 16Q stops conducting. At this time normal operation has been obtained. The only adjustment, 1P is set for 38 volts into the 30 volt series regulator.

The series regulator for the 30 volt supply is shown at the top of the diagram. The other two are identical. Output of the voltage sensing bridge consisting of 15R 16R, 17R, 1P and 2ZD is fed to 7Q and 8Q. An increase in output voltage raises the voltage on 8Q, increasing its conduction and lowering conduction of 7Q. Decreased current in 7Q decreases

current in 4Q, 5Q, and 6Q dropping the output voltage until balance is restored. Excessive current output through 10R turns 3Q on 2Q off, and 1Q on, grounding the base of 7Q. With 7Q off, series regulators 4Q, 5Q, and 6Q are off and the output goes to zero. When 1C discharges, 3Q is turned off and output is restored. The circuit will oscillate between off and on until the cause of the high current is removed.

INSTALLATION AND ADJUSTMENT

The electronic control cabinet should preferably be mounted in a clean dry air conditioned environment. Ambient temperature should not exceed 104° F unless otherwise noted on the outline drawing for a specific unit.

Equipment adjustment and the required test equipment are covered in detail in an alignment diagram and alignment instructions furnished with each unit. See 44D302362 and 44A301479 for typical drawings.

The location of sub assemblies within the cabinet is shown on the internal connection diagram furnished with each control. Printed circuit board locations are shown on sheets 1 and 2 of the elementary diagram, see 44C300886.

OPERATION

Refer to the instruction book for the turbine.

MAINTENANCE

No periodic maintenance is required. Outage time due to component failure is best minimized by maintaining a complete set of spare parts. Elementary diagrams of the printed circuit boards as e included in this instruction book. The assembly drawings showing component location on the printed circuit boards are furnished with each order except where component identifications are silk screened on the boards in which case assembly drawings are not furnished.

TROUBLESHOOTING

Most troubleshooting problems can be quickly isolated to a particular section of the control by use of the built-in test meter, the meter relays, and alarm lights. These used in conjunction with the alignment diagram indicate the operating condition of each section. An oscilloscope is recommended for pinpointing a defective component or components. Each printed circuit board can be removed from the rack for servicing without disconnection due to the use of terminal boards.

RENEWAL PARTS

When ordering renewal parts, address the nearest Apparatus Sales Office of the General Electric Company and supply the following information.

- a. Catalog number stamped on the part and a complete description of the part, including its use and location.
- b. Complete nameplate data appearing on the assembly of which the part is a component.
- c. If possible, data on orginal order on which equipment was first supplied, including all numerical references.

Since operation of a steam turbine-generator is dependent upon operation of the feedpump control, it is suggested that an adequate stock of spare parts be carried on hand to minimize outage time due to component failure.

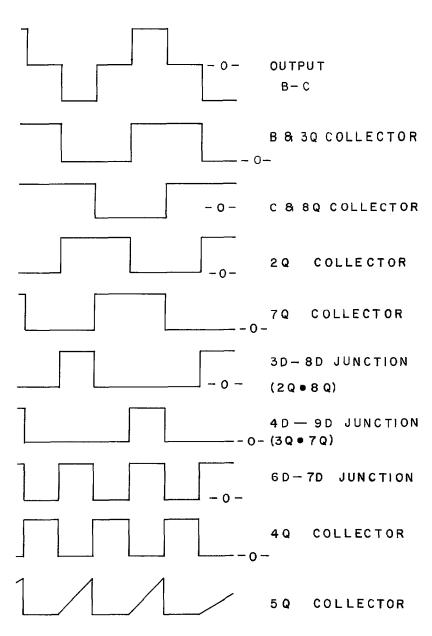
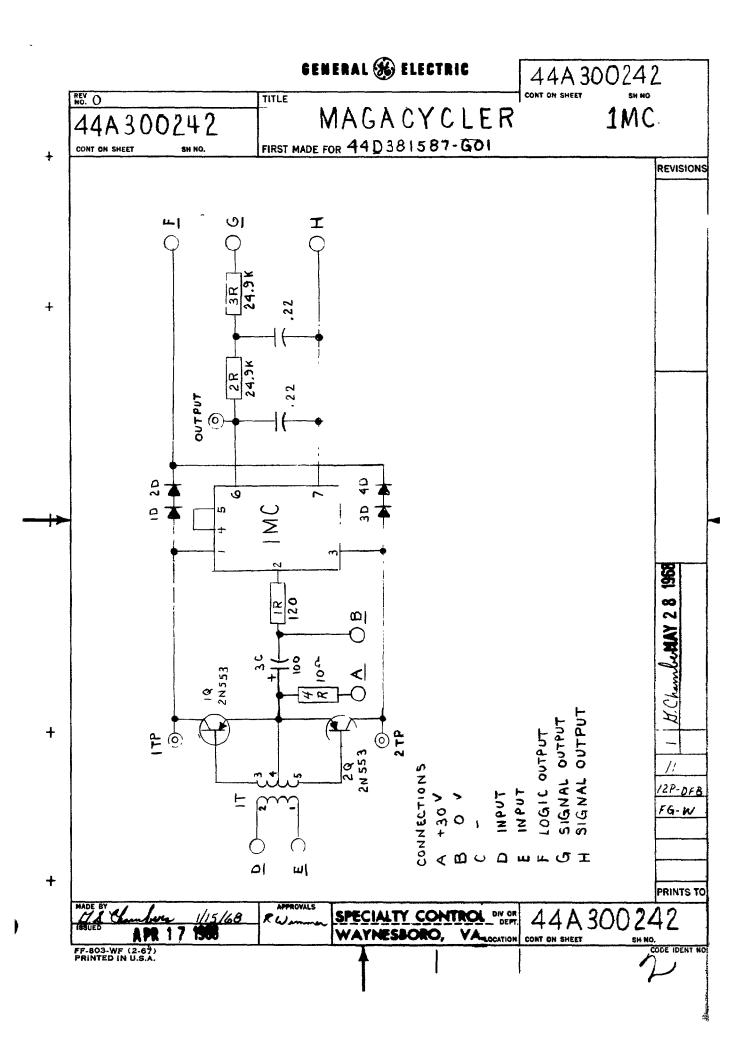
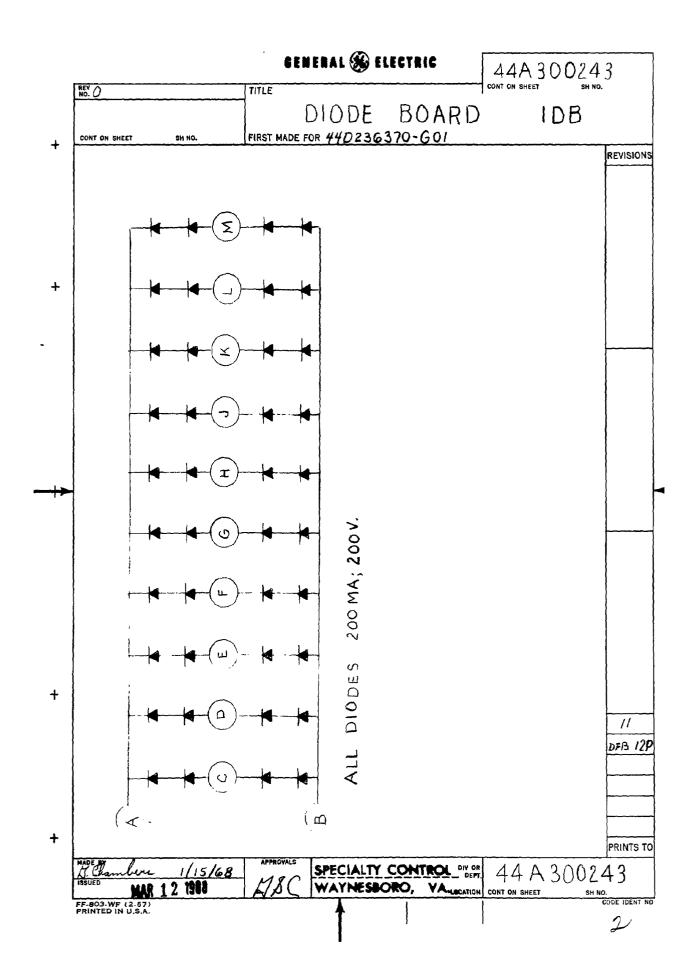
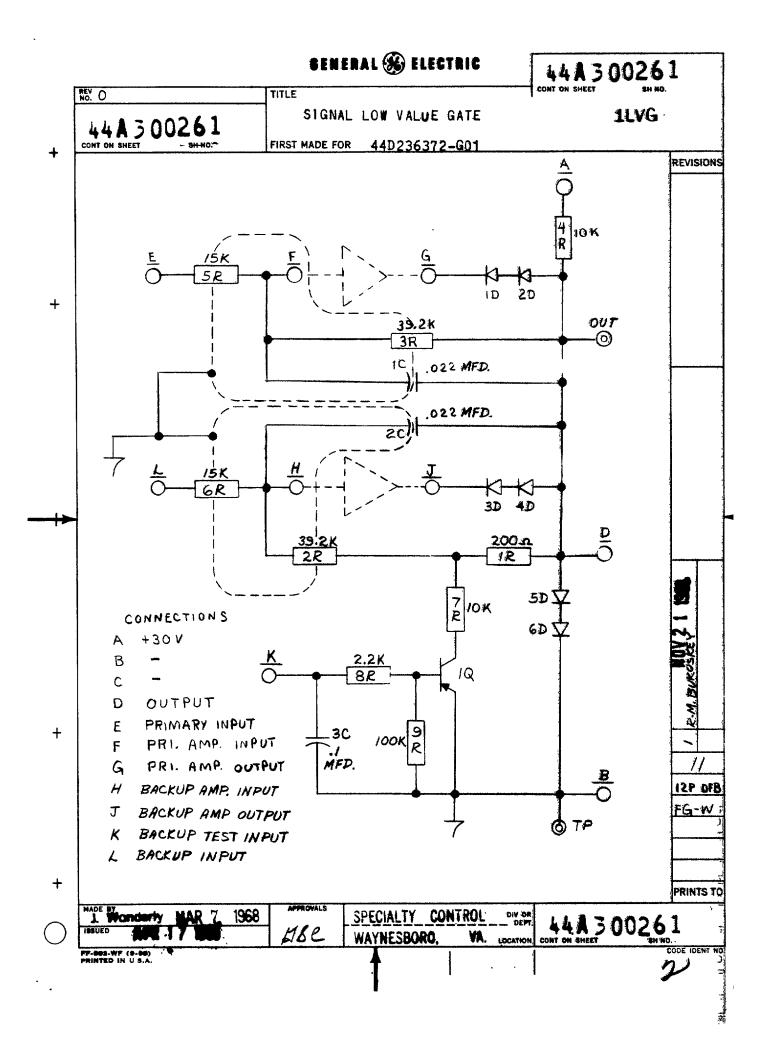
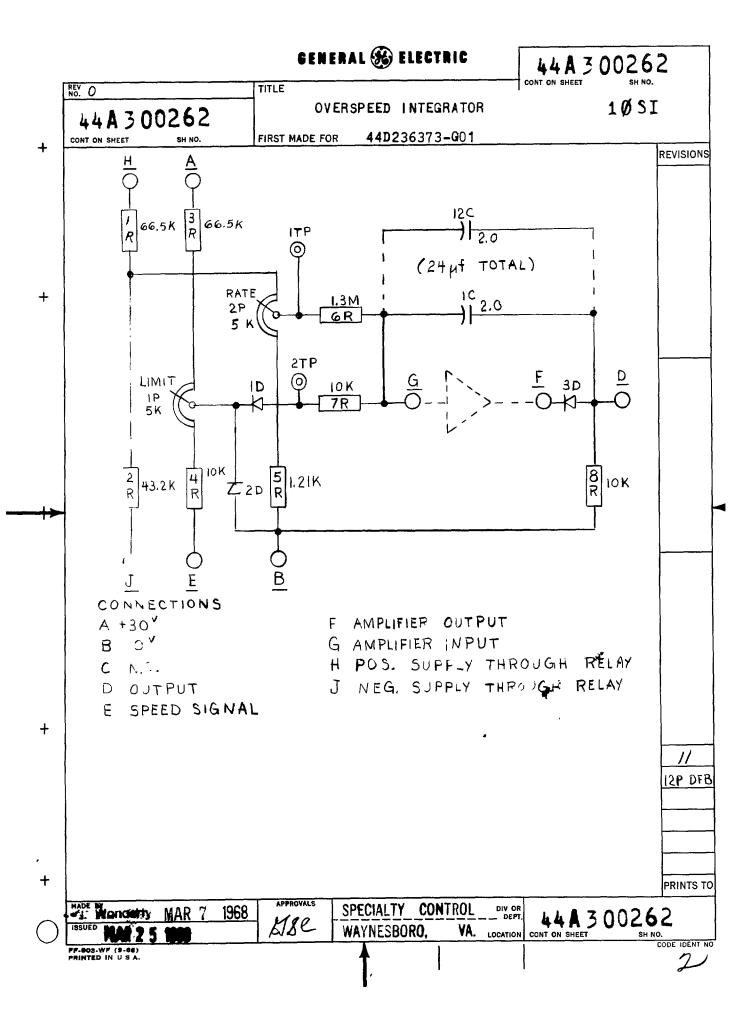


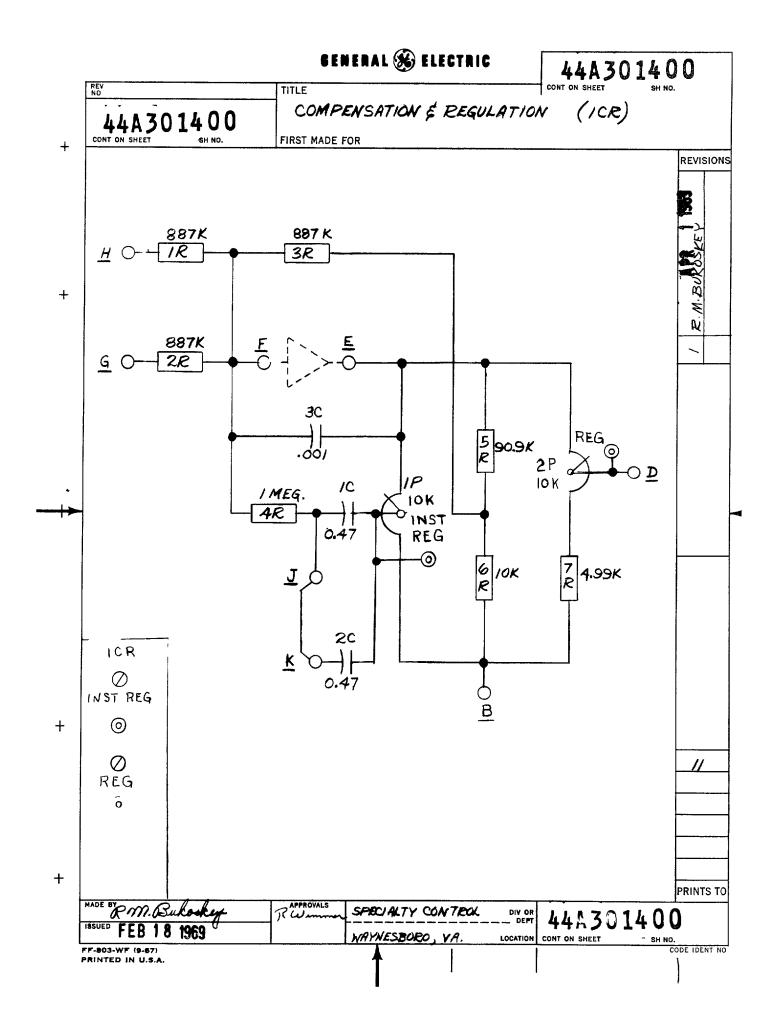
FIG. 3 Inverter Waveforms











GENERAL & ELECTRIC 44A301479 CONT ON SHEET 2 SH NO 1 TITLE ALIGNMENT INSTRUCTIONS ELECTRONIC FEED PUMP TURBINE CONTROL 444301479 FIRST MADE FOR 387513TC300A3, TURBINES 122451 & 122452 CONT ON SHEET 2 SH NO. REVISIONS - CONEMAUGH GROUP -REFERENCE ALIGNMENT DIAGRAM 44D301726 TEST EQUIPMENT AUDIO OSCILLATOR: HEWLETT PACKARD 201C, 200CD; GENERAL RADIO 1210C, OR EQUIVALENT. OUTPUT MUST BE 10 VOLTS RMS MINIMUM INTO 600 OHMS. 2. AC/DC DIGITAL VOLTMETER: 0.1 MV TO 100 V MAX. DIGITAL FREQUENCY COUNTER: 6 VOLT RMS SENSITIVITY. 30 TO 5000 HZ. TEN TURN POTENTIOMETER; NOT MORE THAN 5000 OHMS RESISTANCE. 4. TWO INPUT OSCILLOSCOPE, CALIBRATED SWEEP: X1 AND X10 PROBES. OPTIONAL: BRUSH RECORDER: SPECIAL TESTS ARE DESIRED. 6. VOLT - OHM - MILLIAMMETER 7. PRELIMINARY ١. CHECK INTERCONNECTION OF CONTROL CABINET. OPERATOR'S CONTROL DEVICES, TURBINE DEVICES, ETC. MECHANICALLY ZERO TEST METER IN CABINET AND OPERATOR'S TACHOMETER AND OTHER INSTRUMENTS. LINE POWER SUPPLY 120V. 10. 60HZ.

1. INVERTER OUT: APPLY POWER AND ADJUST INVERTER OUTPUT FOR ш. 38 VOLTS AT D+ & E- IF 1SR, LOC. 0308. THE INVERTERS ARE IN THE BOTTOM OF THE CABINET WITH LINE INVERTER IN BACK AND PMG INVERTER IN FRONT. DC SERIES REGULATORS: ADJUST POWER SUPPLIES AND METER 2. CALIBRATIONS PER CHART LINE SUPPLY TEST POINTS **ADJUST** +30 V BUS BARS 0308 -22V BUS BARS 0316 24V +F LOC. 0322:-G LOC. 0324 0324 METER RELAY ALARMS: VARY ALARM SET POINT OF LINE SUPPLY METER RELAYS TO CHECK ALARM OPERATION. SET ALARMS FOR 95% AND 105%. li 2P-DFB FG-W

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ALIGNMENT INSTRUCTIONS

ELECTRONIC FEED PUMP TURBINE CONTROL

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sh no. 2

FIRST MADE FOR 3\$7513TC300A3, TURBINES 122451 & 122452

3KHZ OSCILLATOR -0222,0225,0228

MEASURE OUTPUT FREQUENCY AT 0228 WITH COUNTER. IF FREQUENCY IS OUTSIDE LIMITS OF 3000HZ ± 30 HZ REMOVE 0222 AND ADJUST REACTOR.

ADJUST VOLTAGE LEVEL FOR 6.000 ± .006V. SET METER FOR 100%. CHECK METER RELAY ALARMS AND SET AT 95 AND 105 PERCENT.

11. PMG SPEED MEASURING CIRCUITS

- FREQUENCY TO VOLTAGE CONVERTER 1FVC. LOC. 0217: ADJUST ZERO FOR ZERO VOLTS TERMINALS D & B.
- SET-UP: REMOVE LEAD FROM J OF 1FVC, 0217 AND CONNECT AUDIO OSCILLATOR AND COUNTER TO THIS POINT AND B.
- TACHOMETER: AT RATED PMG FREQUENCY ADJUST OUTPUT 1. 0217 FOR RATED RPM TACH INDICATION. SEE ALIGNMENT DIAGRAM.
- SET VOLTAGE COMPARATOR, LOCATIONS 0218, 0219, AND 0220 PER ALIGNMENT DIAGRAM. CHECK EACH SETTING BY SLOWLY VARYING FREQUENCY ABOUT THE OPERATING POINT. OBSERVE OPERATION WITH OSCILLOSCOPE CONNECTED TO THE OUTPUT TEST POINTS. RELAY DROPOUT IS O VOLTS AND PICKUP APPROXIMATELY 0.3 VOLTS.
- SECOND TACHOMETER 3A02. LOC. 0121: AT 0 FREQUENCY ADJUST BIAS FOR 0 INDICATION.ADJUST GAIN FOR TACH INDICATION PER ALIGNMENT DIAGRAM.
- REMOVE TEST CONNECTIONS TO 0217 AND RECONNECT LEAD TO TERMINAL J.

٧. SSPU SPEED MEASURING CIRCUITS

- SET-UP: JUMPER T4 TO T7 AND T5 TO T8. CONNECT OSCILLATOR AND COUNTER TO T4 AND T5.
- FREQUENCY TO VOLTAGE CONVERTERS 1MC, LOC, 0202 AND 0205 HIGH SPEED GATE 1LVG. LOC. 0209
- 2.1 PRIMARY: AT RATED SHAFT SPEED PICKUP FREQUENCY ADJUST 1MC. LOC. 0202, FOR -5.000 VOLTS AT OUTPUT TESTPOINT OF 1LVG (OBSERVE WITH TEST METER IN POSITIONS 6 AND 7 THAT AMPLIFIER 7 IS MORE POSITIVE THAN 6; IF NECESSARY ADJUST 1MC, 0205, TO OBTAIN THIS CONDITION.)
- 2.2 BACKUP: DEPRESS BACKUP SPEED AMPLIFIER TEST SWITCH AND ADJUST 1MC, 0205, FOR -5.05 VOLTS AT OUTPUT TP, 0209.

APPROVALS

REMOVE TERMINAL POINT JUMPERS AND OSCILLATOR AND COUNTER 3. LEADS.

2P-DFB2

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44A30 1479 CONT ON SHEET 4 SH NO 3 REV TITLE ALIGNMENT INSTRUCTIONS 44A30 1479 ELECTRONIC FEED PUMP TURBINE CONTROL CONT ON SHEET 4 SH NJ 3 FIRST MADE FOR 357513TC300A3. TURBINES 122451 & 122452 REVISIONS VI. CONTROL VALVE RAM SERVO LOOP CHECK LVDT CORE PER LEVER DIAGRAM. DETECTOR INDICATOR 1DI, LOC. 0216.: WITH CONTROL VALVE FULL OPEN ADJUST NULL OF 1DI FOR 0.00 ± 0.01 VOLTS AT OUT TP. NOTE VOLTAGE READING ON ALIGNMENT DIAGRAM. WITH VALVE IN CLOSED OVERTRAVEL POSITION RECORD OUT TP VOLTAGE ON ALIGN. DIAG. ADJUST ZERO FOR O INDICATION OF CONTROL VALVE POSITION ON OPERATOR'S CONTROL CONSOLE. RETURN VALVE TO FULL OPEN POSITION AND ADJUST CALIBRATE FOR 100% POSITION INDICATION. DETERMINE GAIN OF DETECTOR CIRCUIT IN VOLTS PER INCH BY DIVIDING THE DIFFERENCE IN OUT TP VOLTS AT EXTREME VALVE POSITIONS BY THE TOTAL VALVE TRAVEL IN INCHES, AND RECORD THIS FIGURE ON THE ALIGNMENT DIAGRAM. MAKE ELECTRICAL CONNECTIONS TO SERVO VALVE. 4. SERVO AMPLIFIER, 2SA, LOC. 0214: PS10 TRIP: CHECK FOR APPROX. -0.7 VOLTS AT "I" TP UNDER 5.1. TRIP CONDITION. CLOSE SIGNAL CHECK: WITH TURBINE TRIPPED, DISCONNECT DEMAND 5.2 TERMINAL E AND LIFT TERMINAL D OF 2SA. CONNECT TEST POT WITH NEGATIVE OUTPUT TO TERMINAL D AND SET POT FOR ABOUT -3 VOLTS AT LIFT TP. THE OUTPUT OF AMPLIFIER 9 ON TEST METER POSITION 9 SHOULD BE ABOUT -10 VOLTS. TURN BIAS ADJUSTMENT CCW UNTIL AMP. 9 GOES TO +10 VOLTS. THERE SHOULD BE LITTLE OR NO CONTROL OF 9 AT INTERMEDIATE VOLTAGES. LEAVE 9 AT +10 VOLTS AND RESET TURBINE. SI REDUCE TOWARDS 0 THE TEST POT SETTING AND NOTE THAT 9 SWINGS FROM +10 TO A MINIMUM VALUE OF APPROX. -6.2 VOLTS. NOW APPLY MORE MEGATIVE VOLTAGE FROM THE TEST POT AND NOTE THAT 9 HAS A MAXIMUM VALUE OF APPROX. +6.2 VOLTS. GAIN: DETERMINE "V" VOLTS LIFT/VOLT I FROM ALIGNMENT 5.3 DIAGRAM. VARY THE TEST POT SETTING UNTIL I TP IS 0.000 VOLTS AND NOTE LIFT TP VOLTAGE. CHANGE THIS VOLTAGE WITH THE TEST POT BY +V VOLTS. ADJUST GAIN UNTIL I TP READS -1.000 VOLTS. RECHECK O POINT, THEN CHANGE LIFT VOLTAGE BY -V VOLTS AND NOTE THAT I TP IS +1.000 VOLTS. BLAS: DISCONNECT TEST POT AND RECONNECT THE LEAD REMOVED 5.4 FROM D. WITH THE VALVE IN THE CLOSED OVERTRAVEL POSITION ADJUST BIAS FOR -0.035 VOLTS AT I TP. RECONNECT TERMINAL Ε. 11 AFTER REMOVING THE ELECTRICAL CONNECTOR, MOUNT THE SERVO VALVE AND VERIFY THAT THE MECHANICAL BIÁS IS IN THE VALVE 2P-DFB CLOSING DIRECTION. FG-W +PRINTS TO APPROVALS COMM. & CONTROL DIV OR Morra 7-2 69 -DEVICES -DEPT .--- DEPT 44A301479 ISSUED

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1.	ULATION AND CON REGULATION: SUE NEGATIVE SUPPL ADJUST REGULATION TO FULL LOST THE TEST PO	BSTITUTE TH _Y FOR THE TION TO OBT _OAD LIFT FO	E OUTPUT OF CONNECTION TO AIN VALVE TR	THE TEST I D TERMINAI AVEL FROM	L E. EFFECTIVE	·UT	
2. 3.	COMPENSATION: ALIGNMENT DIAC INSTANTANEOUS AND ADJUST INSTANTION PER	VERIFY THAT GRAM. REGULATION ST. REG. FO	SET TEST POT R A VOLTAGE	T FOR 1 V	OLT OUTPUT		
111 - MANU	UAL SPEED REFRE THIS REFERENCE MOTOR DRIVEN L	E <mark>NCE</mark> (STAND E IS OBTAIN	-STILL CHECKS ED FROM THE	UPPER OF	THE TWO	IN	
2.	TO LSS AND LIC SLOW REFERENCE PRESSURE OIL S RAISING MANUAL	GHT THE LSS E <u>SPEED, 2C</u> SUPPLY OR D L REFERENCE	INDICATING I L. LOC. 0116 ISCONNECT SEI . ACTUATE R	_IGHT. _: SHUT OF RVO VALVE AISE PUSH	FF HIGH BEFORE BUTTON AND) IV	
3.	TIME TRAVEL TO 80-90 SECONDS. MEASURED AT CL FAST REFERENCE ACTUATE LOWER HSS LIGHT TO L	. A CLOCK LOCK TP. E SPEED, 20 FAST PUSHB	PERIOD OF 40 L. LOC. 0116 UTTON AND TI	MILLISEC ME MOTOR	ONDS CAN BE		
4.	A CLOCK PERIOD CLOCK TP WHILE BIAS AND GAIN DISCONNECT K CAND BACK INTO	D OF 4.17 M E LOWER FAS MANUAL RE OF 2LVG. R	ILLISECONDS T PUSHBUTTON FERENCE, 2LV AISE MANUAL	CAN BE ME IS ACTUA G <u>, LOC. O</u> RÉFÉRENCE	ASURED AT TED. 113: FROM LSS		
1X. <u>AUTC</u> 1.	ADJUST MANUAL RAISE TO HSS A OUTPUT VOLTAGE DIAGRAM. DSPEED REFERENCE SET-UP: AUTO F T31 TO T32 ANI LEAD FROM THE FIRST, HOWEVER HSS, LSS 2SC	BIAS FOR O AT SLOW RAT E AT TP 011 CE (STAND REFERENCE C D TO LSS BY BOILER CON	.000 VOLTS A E AND ADJUST 3 AS SPECIFI -STILL CHECK AN BE RUN TO JUMPING T31 TROLLER SHOU	T OUTPUT MANUAL GED BY ALIVED BY ALIVED BY TO T33.	TP, 0113. AIN FOR GNMENT UMPING THE EXTERN	N AL	
_,	WITH AUTO REFE TRAVEL TO HSS. SECONDS USING	ERENCE AT L • TRAVEL T	SS, JUMPER T IME SHOULD B	E ADJUSTE	AND TIME D TO 40]/
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GENERAL (%) ELECTRIC 44A30 1479 CONT ON SHEET 6 SH NO 5 TITLE ALIGNMENT INSTRUCTIONS 44A30 1479 ELECTRONIC FEED PUMP TURBINE CONTROL CONT ON SHEET 6 SH NO 5 FIRST MADE FOR 3S7513TC300A3, TURBINES 122451, & 122452 + REVISIONS AUTO SPEED REFERENCE INDICATION, 1DI, LOC. 0128: З. ADJUST ZERO AT LSS AND CAL AT HSS TO OBTAIN 0 AND 100 INDICATIONS ON OPERATOR'S POSITION INDICATOR. 3AO2, LOC. 0121: AT HSS ADJUST GAIN OF 1BCI FOR 1MA AT 3.1. 2A OUT TP. AUTO SPEED REFERENCE STOPS, LSS, 2LVG, LOC, 0113: DISCONNECT G, 0113 AND WITH AUTO REFERENCE AT LSS ADJUST SC BIAS, 0113 FOR OUTPUT TEST POINT VOLTS PER ALIGNMENT 4. DIAGRAM. HSS. 2LVG. LOC. 0113.: WITH AUTO REFERENCE AT HSS ADJUS SC GAIN, 0113 FOR OUTPUT TEST POINT VOLTS PER ALIGNMENT 0113.: WITH AUTO REFERENCE AT HSS ADJUST + 5. DIAGRAM. RECONNECT G. LOCAL/REMOTE CONTROL LIGHT, 1VC, LOC. 0114. ADJUST REFERENCE, 0114 FOR 6.5 VOLTS AT L TP. CHECK THA LOCAL CONTROL INDICATION IS OBTAINED WHEN AUTO REFERENCE CHECK THAT IS AT LSS AND MANUAL REFERENCE IS BELOW APPROXIMATELY 50% POSITION. OVERSPEED TEST INTEGRATOR, RSPEED TEST INTEGRATOR, 10SI, LOC. 0109
RATE: CONNECT VOLTMETER TO OUTPUT TEST POINT 2LVG, 0113.
WITH MANUAL AND AUTO REFERENCE AT HSS, ACTUATE OVERSPEED Χ. TRIP TEST PUSHBUTTON. VOLTMETER READING SHOULD INCREASE 0.6 \pm 0.1 VOLTS PER MINUTE FOR 12 \pm 2% SPEED INCREASE PER MINUTE. ADJUST RATE, 0109 AS REQUIRED. LIMIT: CONNECT OSCILLATOR AND COUNTER TO T4 AND T5. FREQUENCY FOR 120% SSPU FREQUENCY. OVSERVE OUTPUT OF AMPLIFIER 5 WITH TEST METER. ACTUATE OTT PUSHBUTTON AND ADJUST LIMIT, 0109 FOR POINT AT WHICH AMPLIFIER SWITCHES FROM POSITIVÉ SATURATION TO ZERO VOLTS. CHECK BY REDUCING OSCILLATOR FREQUENCY AND SLOWLY INCREASING IT TO THE SWITCHING POINT FREQUENCY. 120% SPEED INDICATION, IVC, LOC, 0210.:
WITH OSCILLATOR AT 120% SSPU FREQUENCY ADJUST REFERENCE, FOR DROPOUT. CHECK BY VARYING FREQUENCY. HIGH SPEED REFERENCE LIGHT, LVC, LOC, 0115.:
ADJUST REFERENCE OF 1VC FOR +5 VOLTS. CHECK FOR DROPOUT AT OUTPUT TEST POINT WHEN AMPLIFIER 5 SWITCHES UPON ACTUATING OTT. + 11 /2P-DFB FG-W + PRINTS TO APPROVALS COMM. & CONTROL DEVICES DEPI

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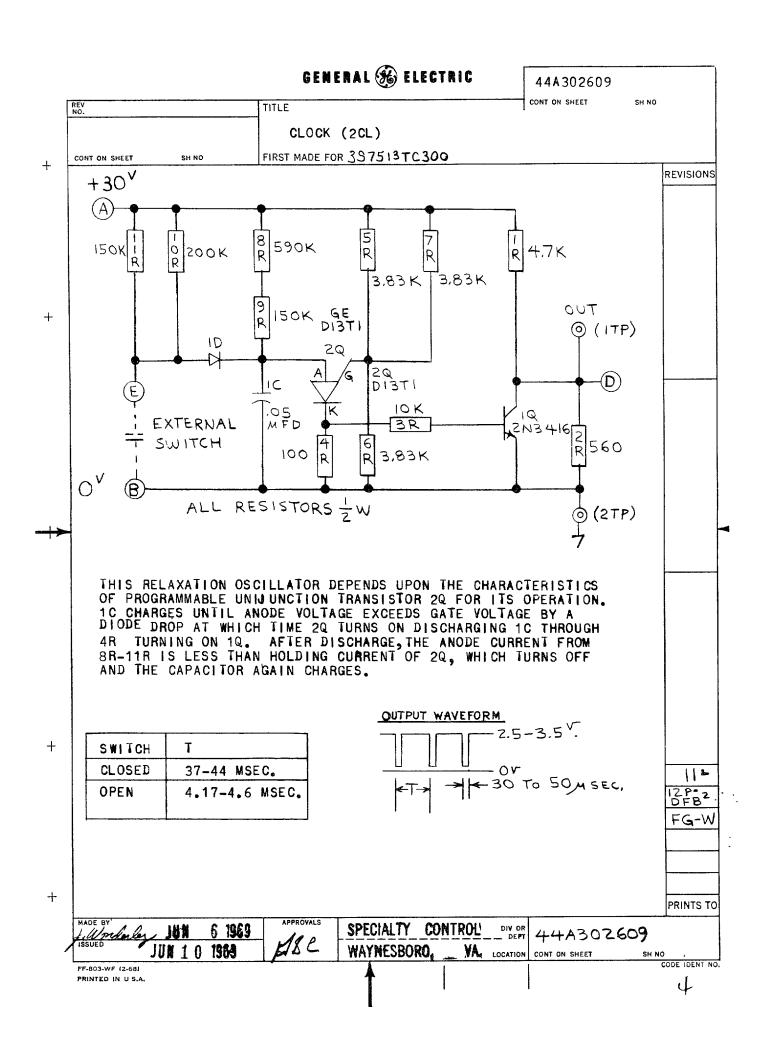
LOCATION CONT ON SHEET 6

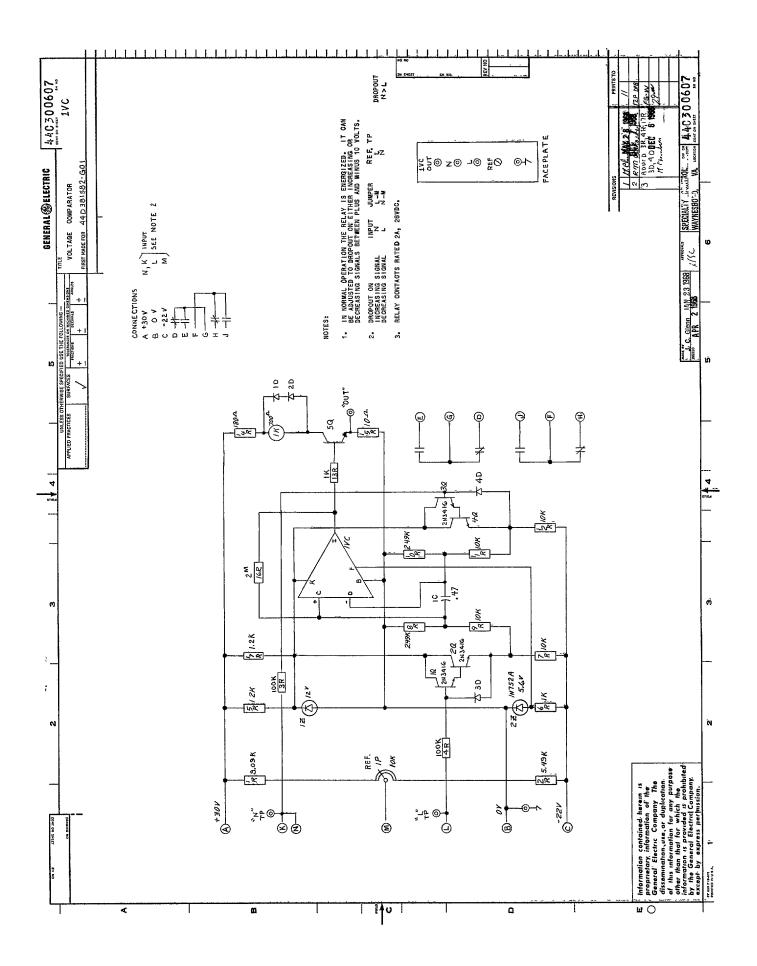
44A301479 CONT ON SHEET FNL. SH NO 6 TITLE ALIGNMENT INSTRUCTIONS 44A301479 ELECTRONIC FEED PUMP TURBINE CONTROL CONT ON SHEET FNL SH NO 6 FIRST MADE FOR 3S7513TC300A3, TURBINES 122451 & 122452 REVISIONS XI. STOP VALVE POSITION INDICATOR, [DI, LOC. 0102. WITH STOP VALVE FULLY CLOSED ADJUST DIFF. TRANS. NULL FOR -3 VOLTS AT OUT TP AND METER ZERO FOR O POSITION. ADJUST CAL. FOR 100% WITH VALVE FULL OPEN. XII.PMG POWER SUPPLY INVERTER ADJUSTMENT: WITH THE TURBINE RUNNING AT 70 TO 100% RATED SPEED ADJUST THE PMG INVERTER (BOTTOM FRONT) FOR 38 VOLTS MEASURED AT D+ AND E-, 1SR, LOC. 0310. + ADJUST THE INDIVIDUAL POWER INDIVIDUAL POWER SUPPLIES: 2. SUPPLY LEVELS UNTIL THE LINE SUPPLIES ARE CARRYING ONLY 0.1 AMPS AND THE PMG SUPPLIES ARE CARRYING THE REST OF THE LOAD. WHILE NOTING THAT THIS CONDITION IS MAINTAINED MAKE FINAL VOLTAGE LEVEL AND METER CALIBRATION ADJUST-MENTS. ALSO TEST AND SET METER RELAY ALARMS AT 95 AND 105%. TEST POINTS SUPPLY LOCATION LINE PMG. 0310 0308 BUS BARS +30 BUS BARS 0316 -22 0318 PMG-+F, 0328; -G, 0326 0326 0324 24 LINE +F, 0322; -G, 0324 SEE LEVER DIAGRAM FOR RUNNING CHECKS OF SPEED REGULATION. $X \square \square$ HP STOP VALVE POSITION INDICATOR 1D1, LOC. 0104. X + VSAME AS XI. 12P-DFB FG-W PRINTS TO COMM. & CONTROL DEVICES DEPI. APPROVALS DIV OR 44A30 1479 6 LOCATION CONT ON SHEET FNL

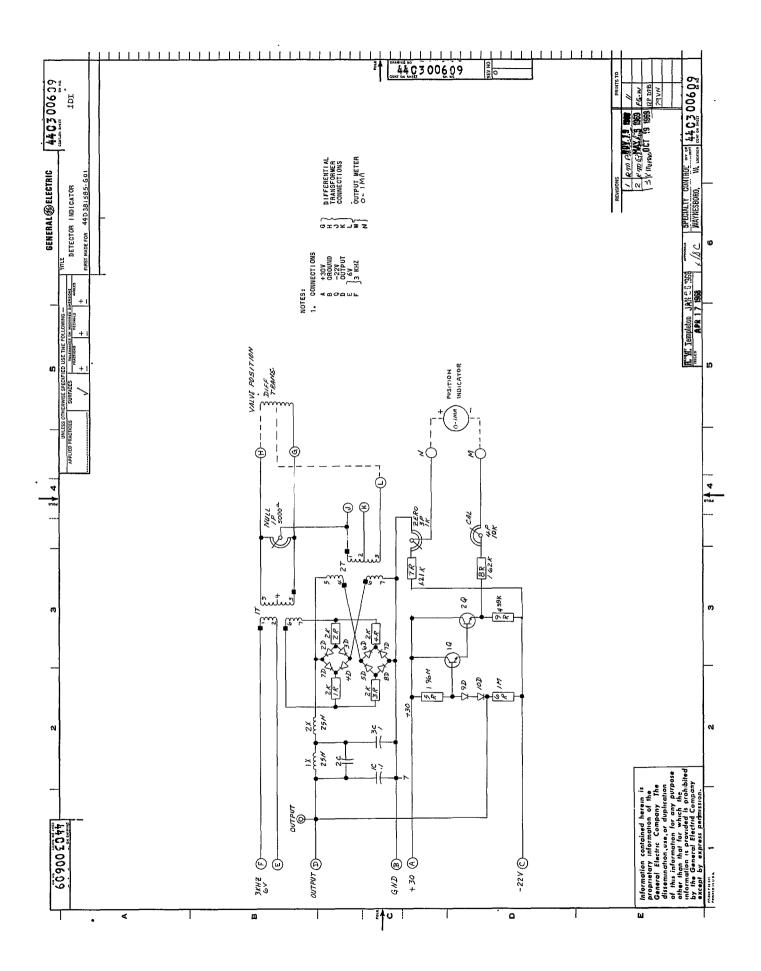
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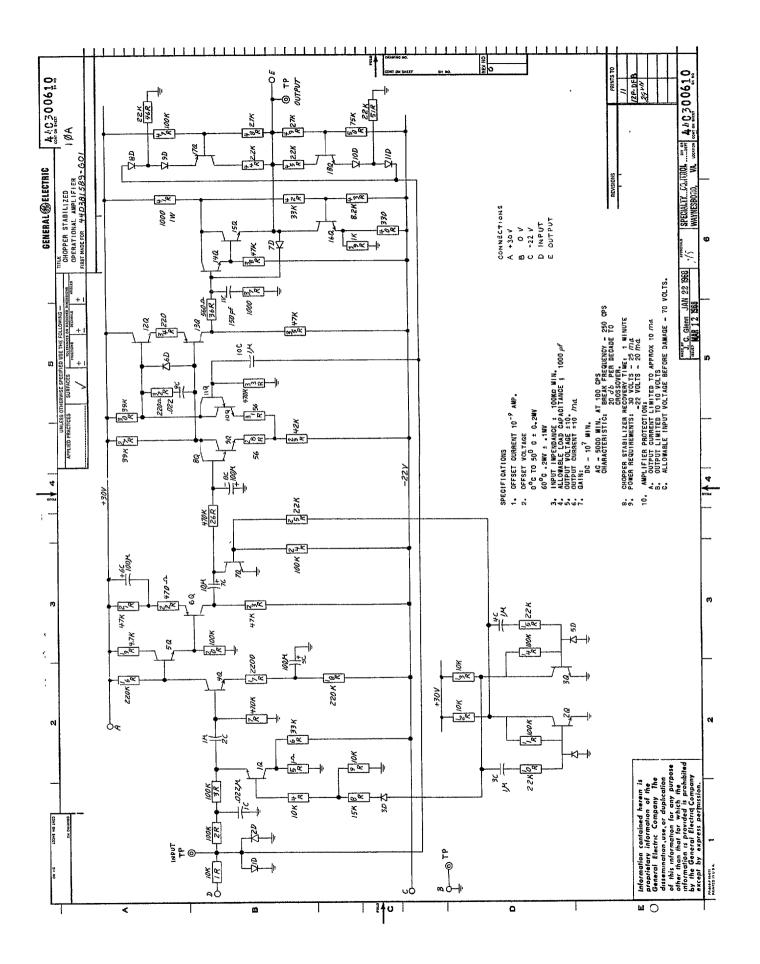
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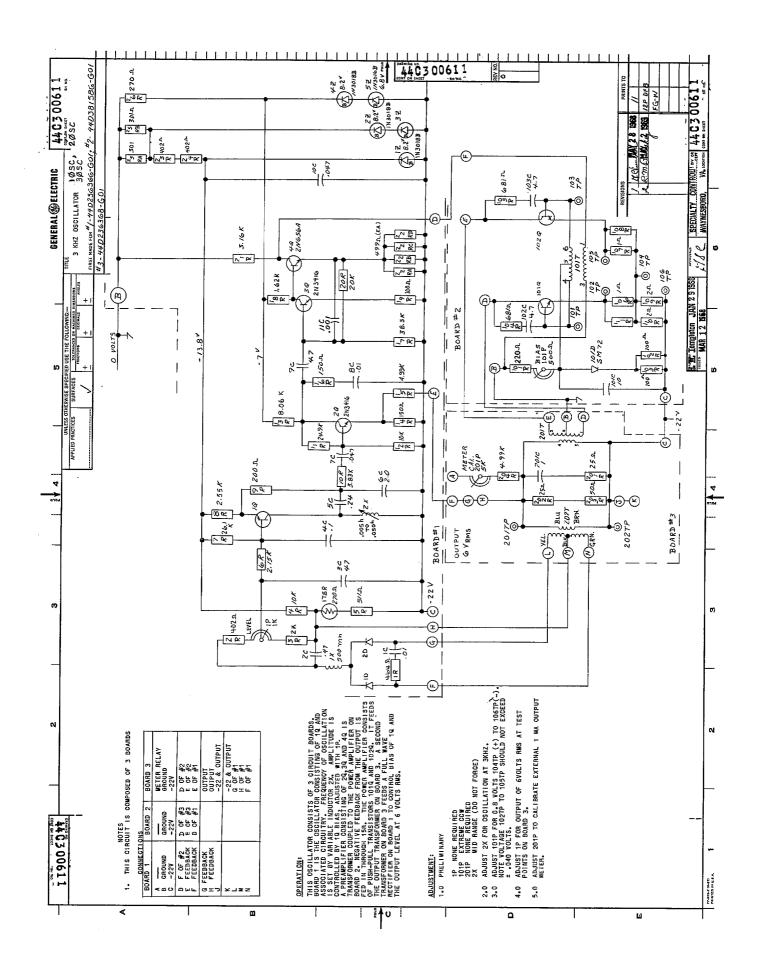
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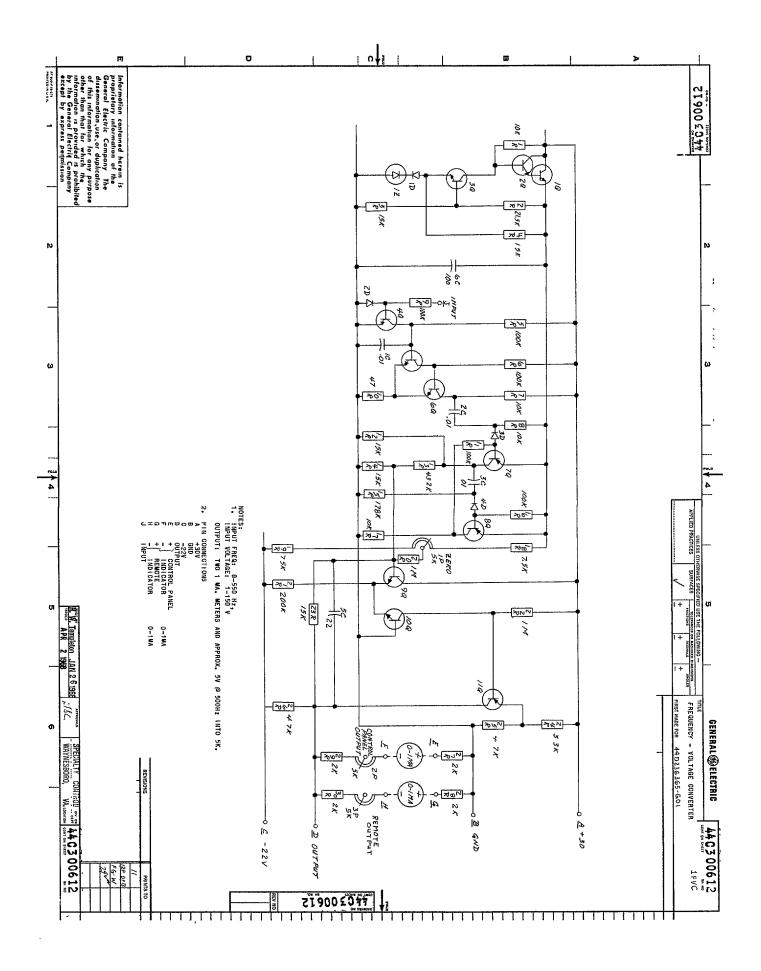


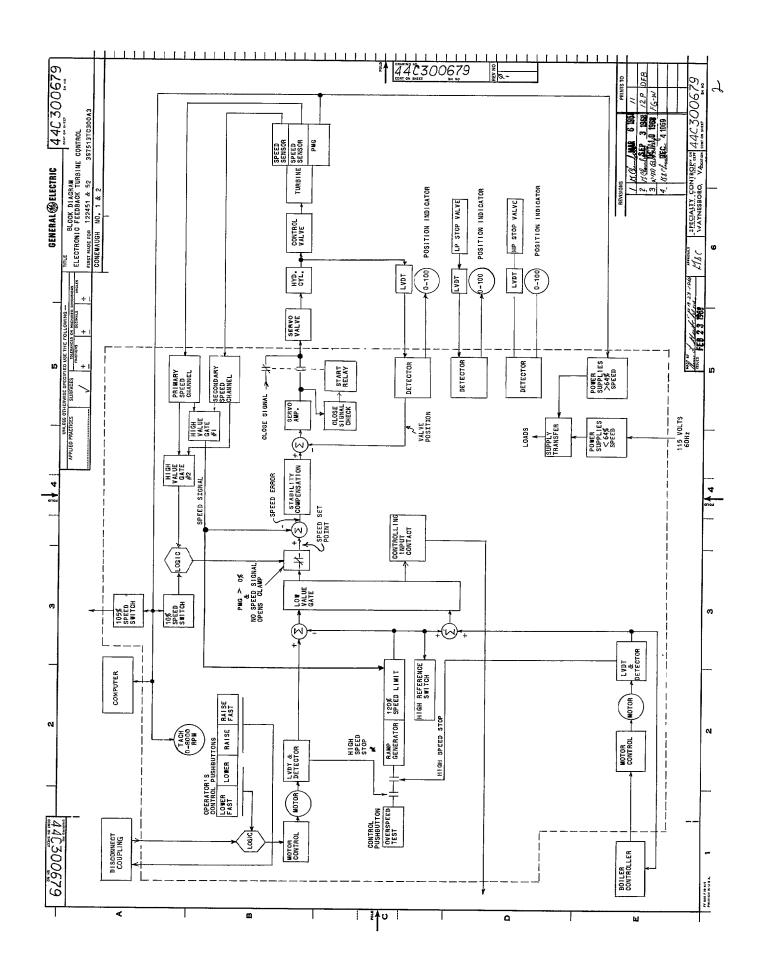


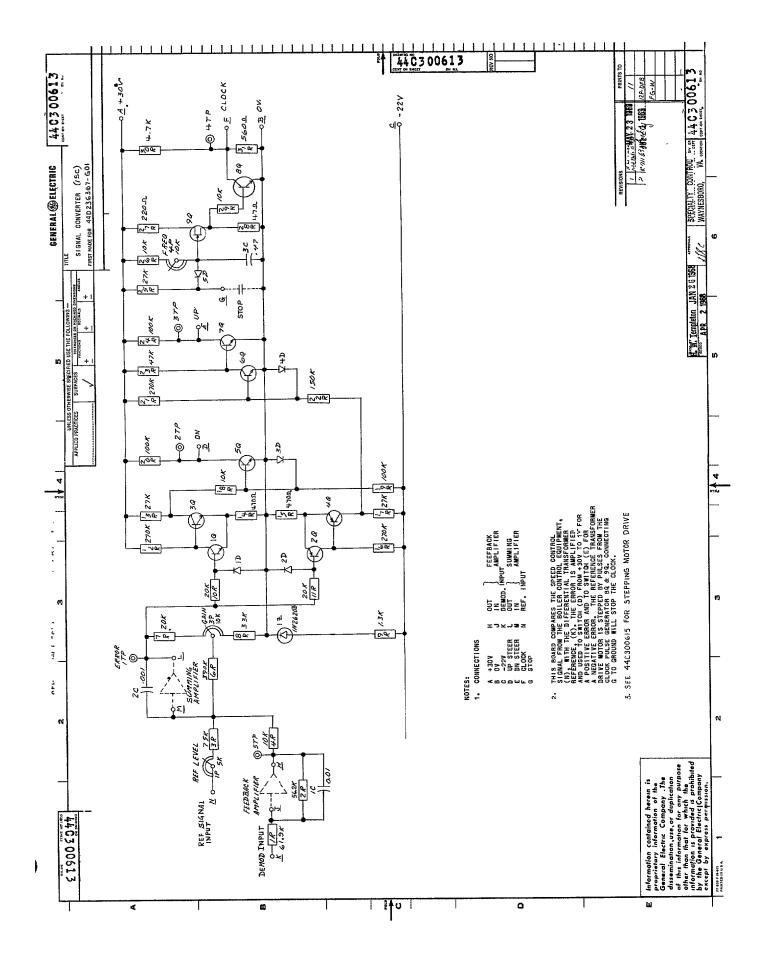


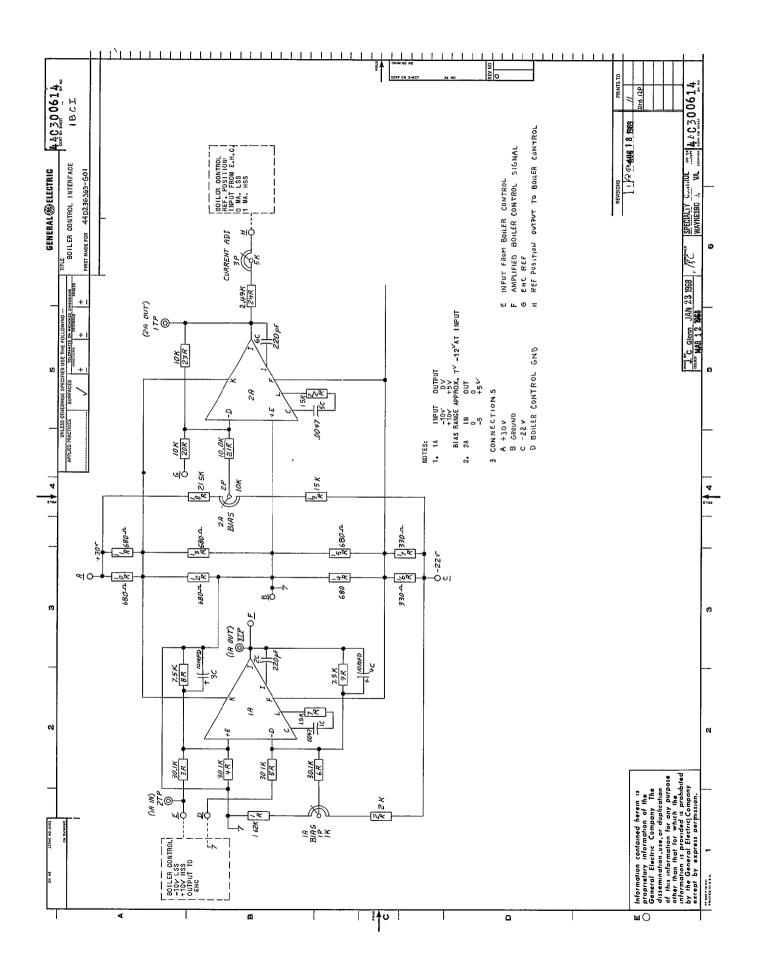


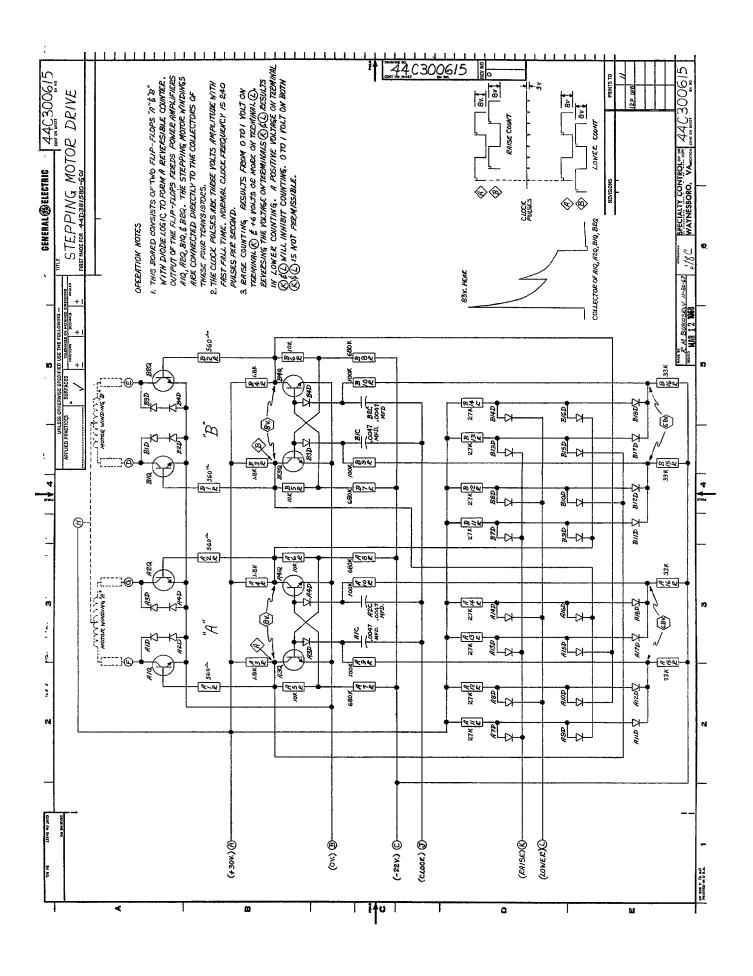


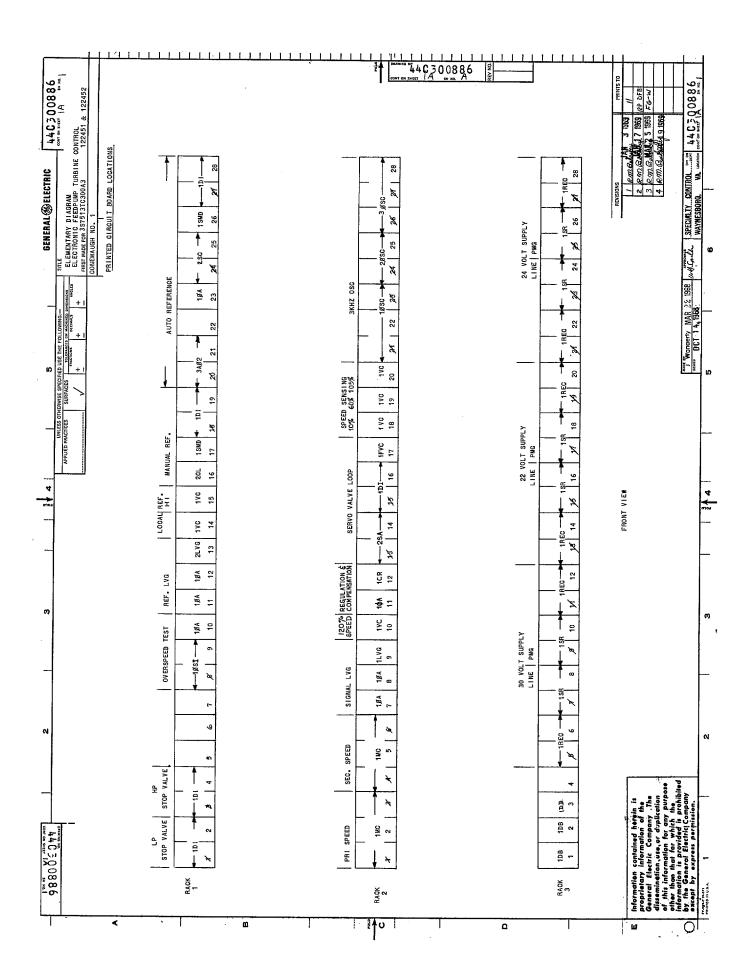


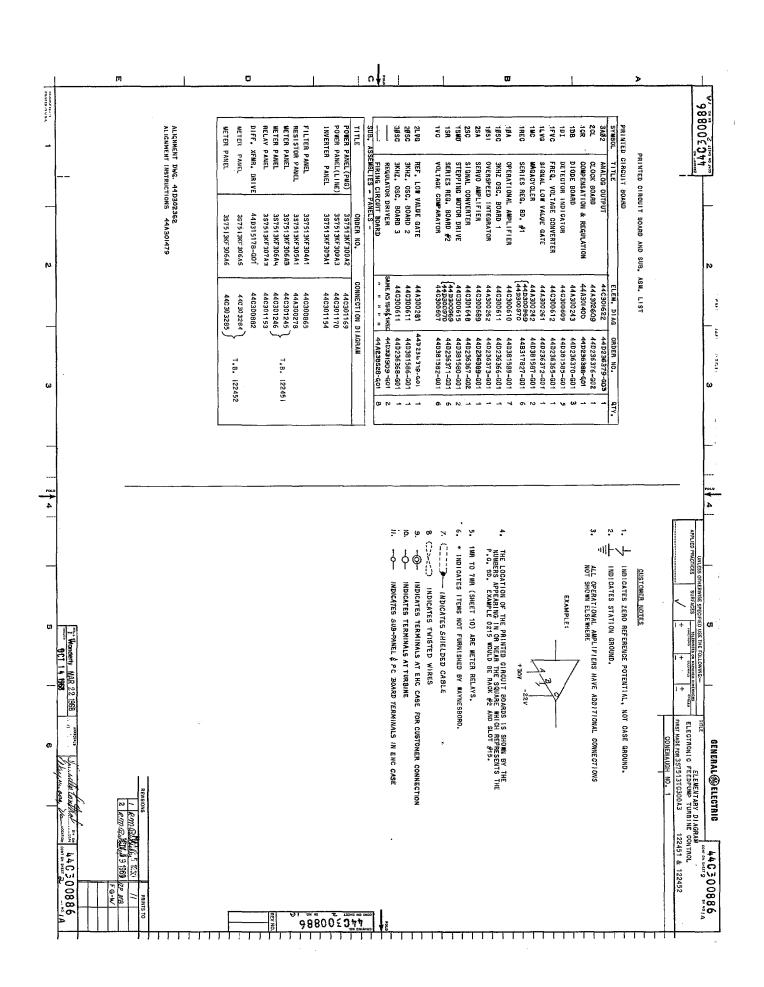


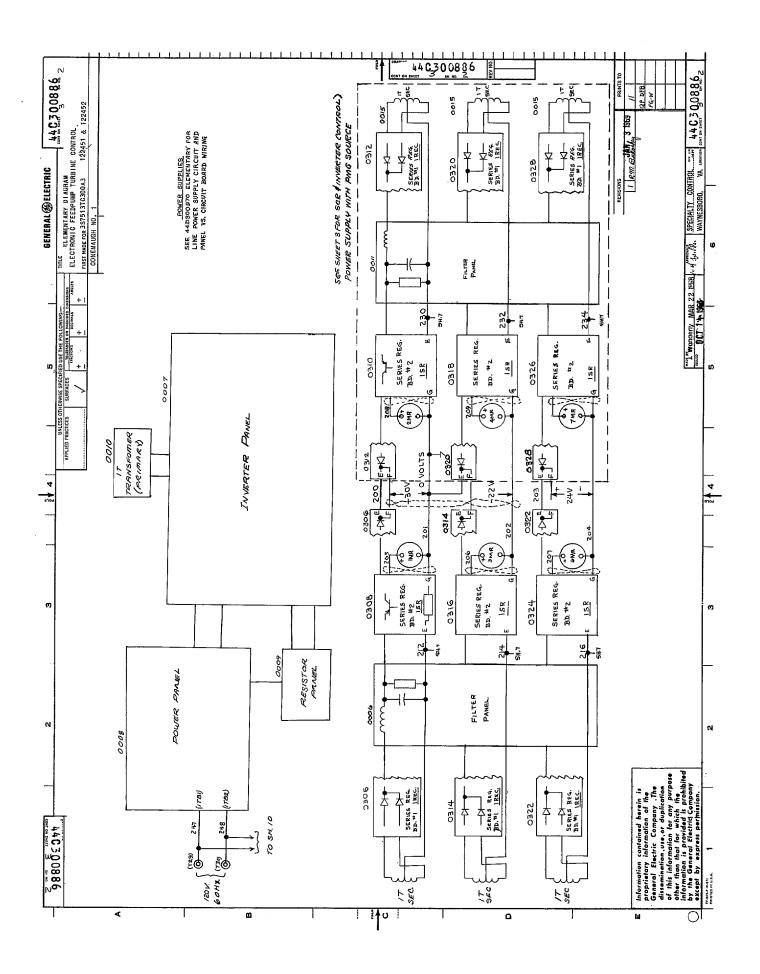


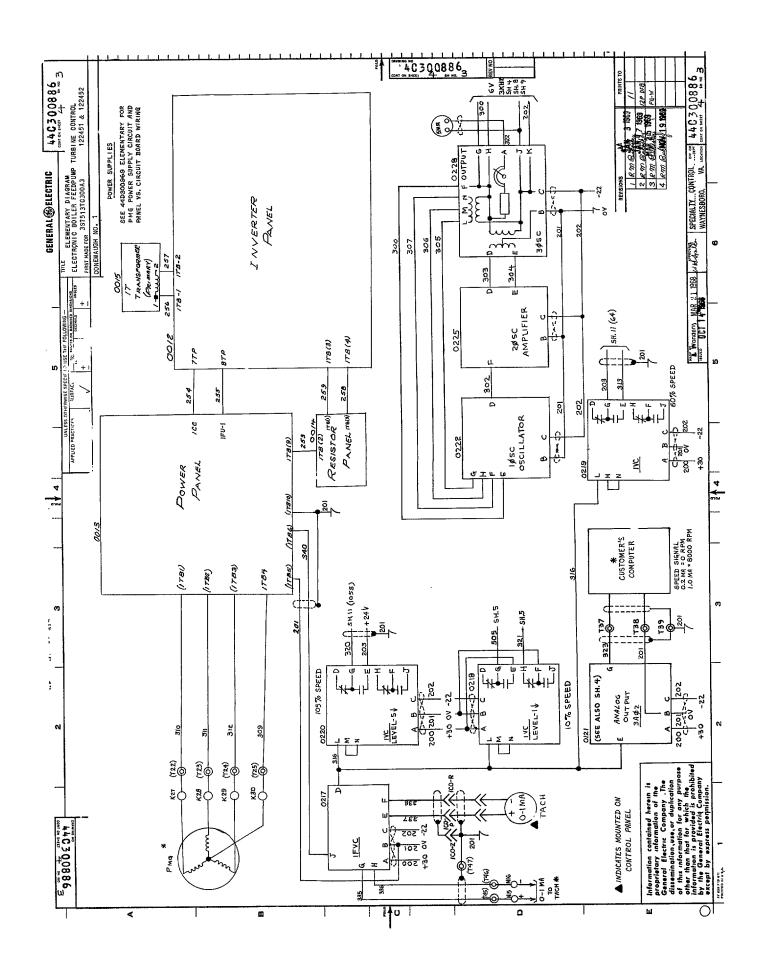


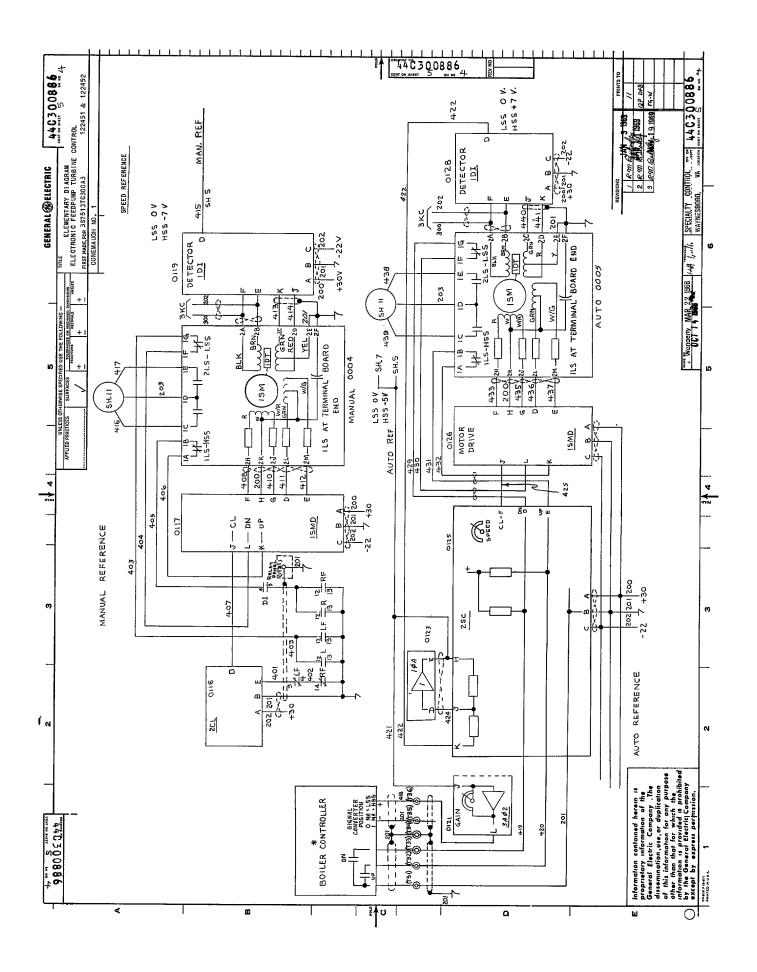


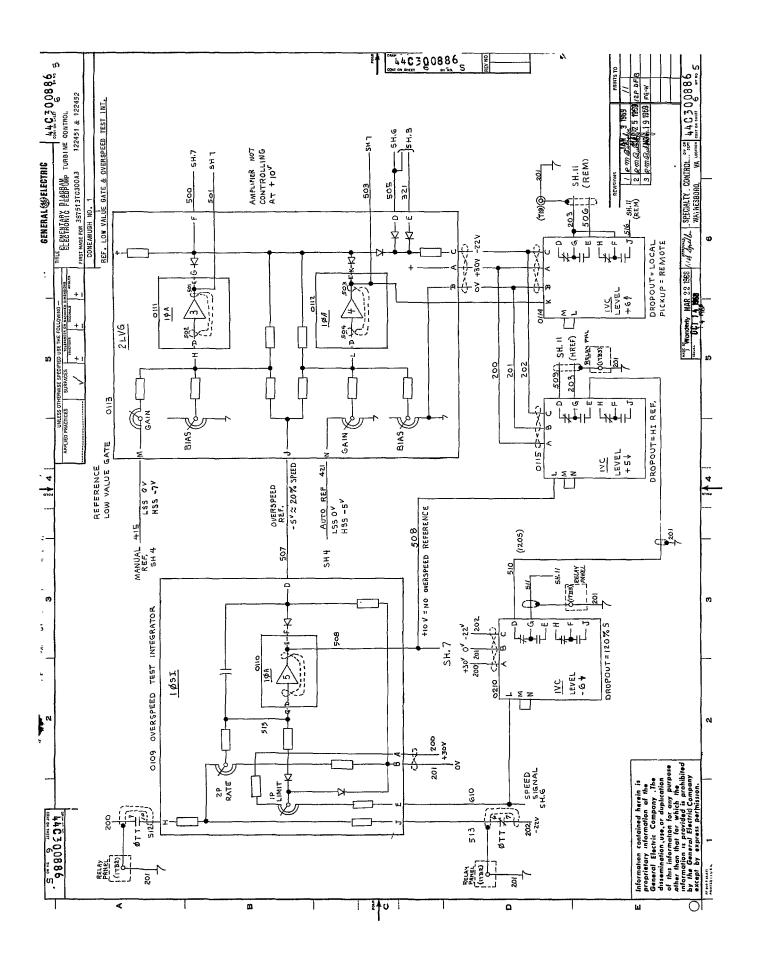


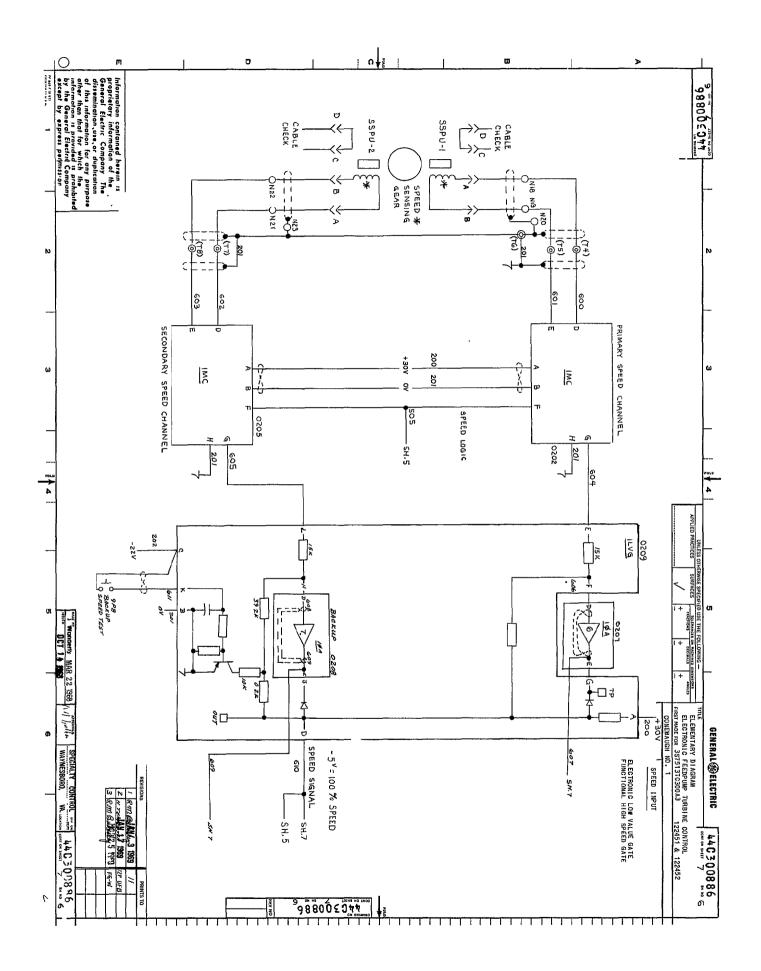


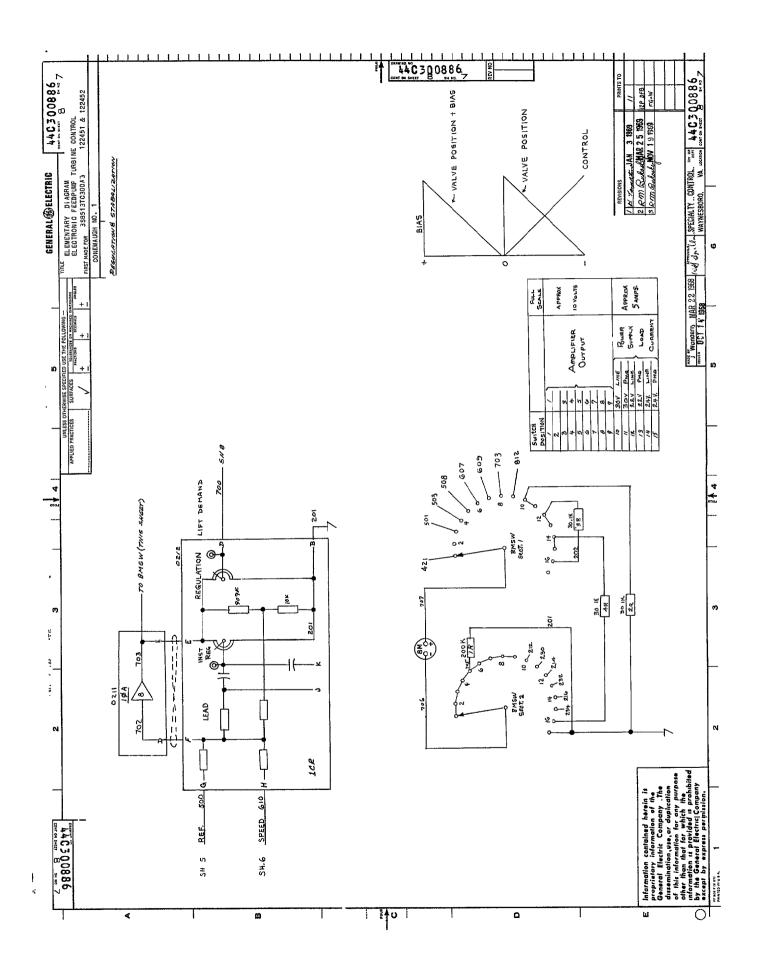


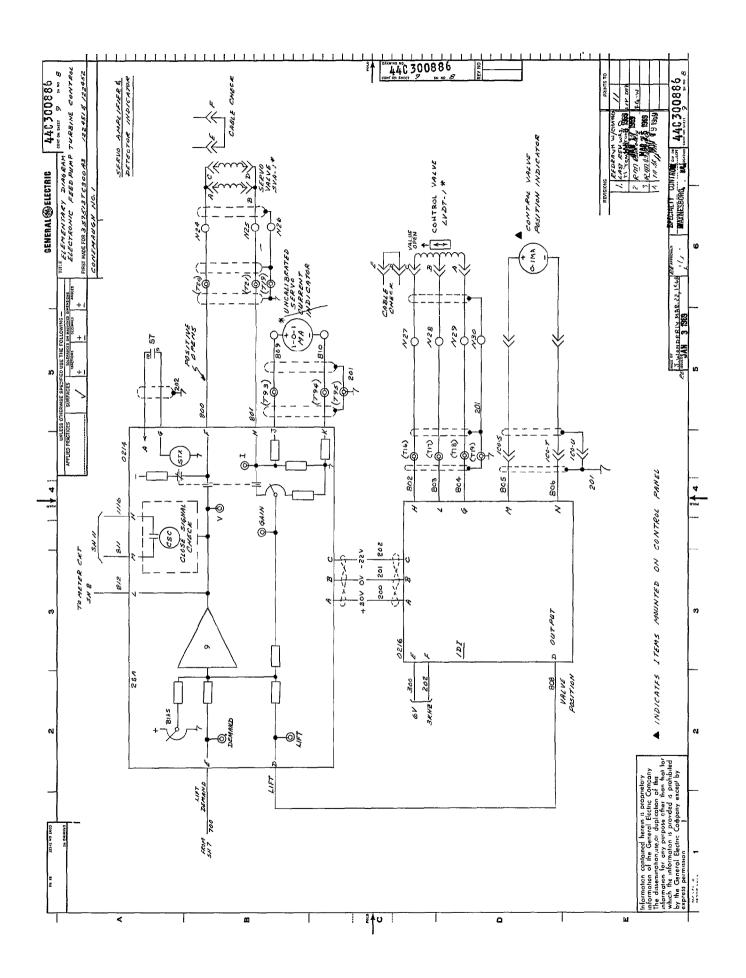


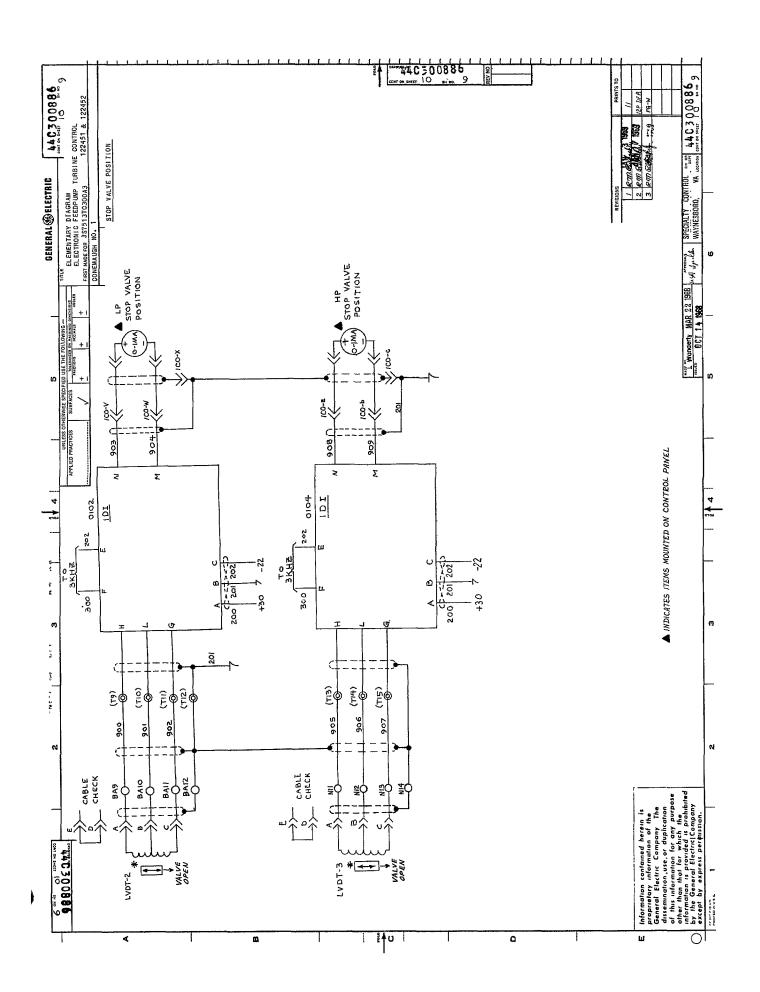


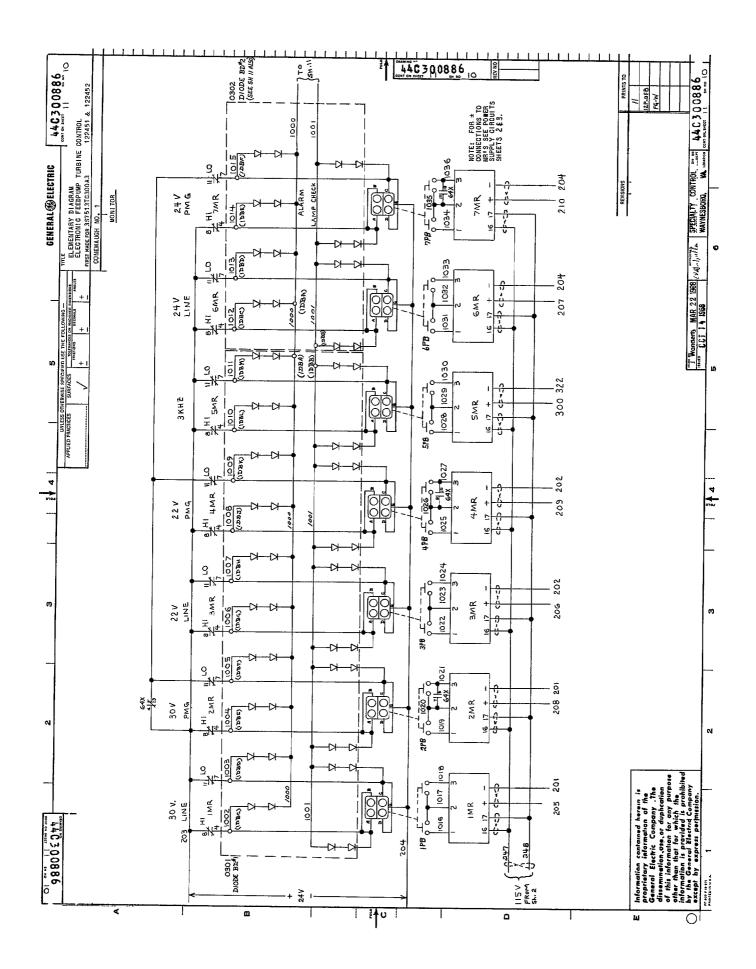


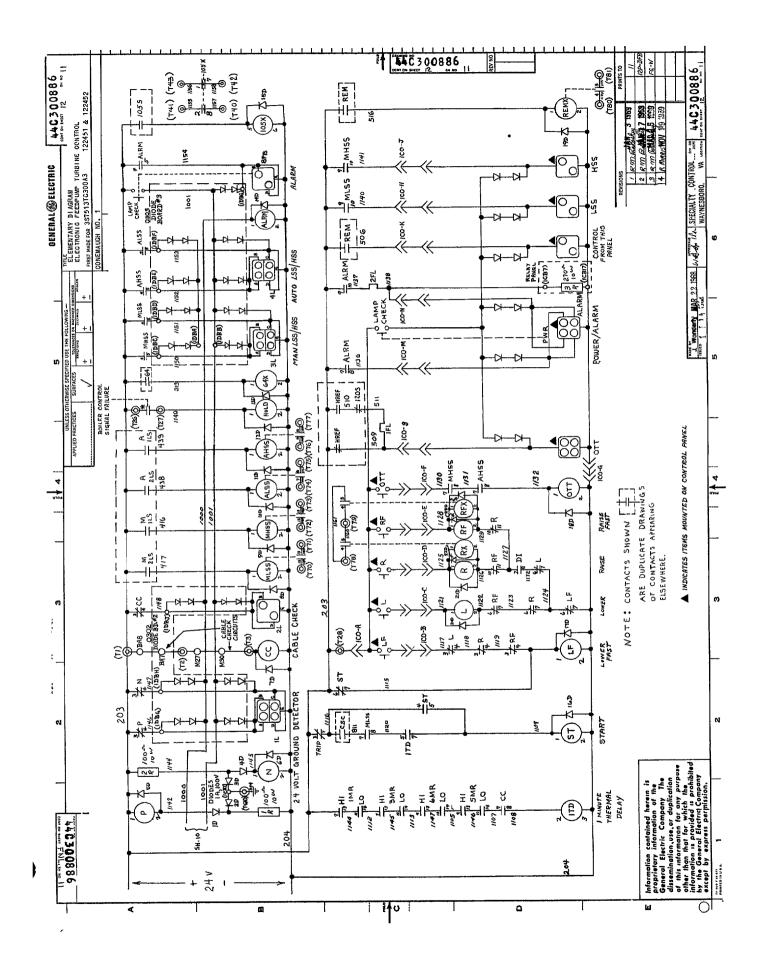


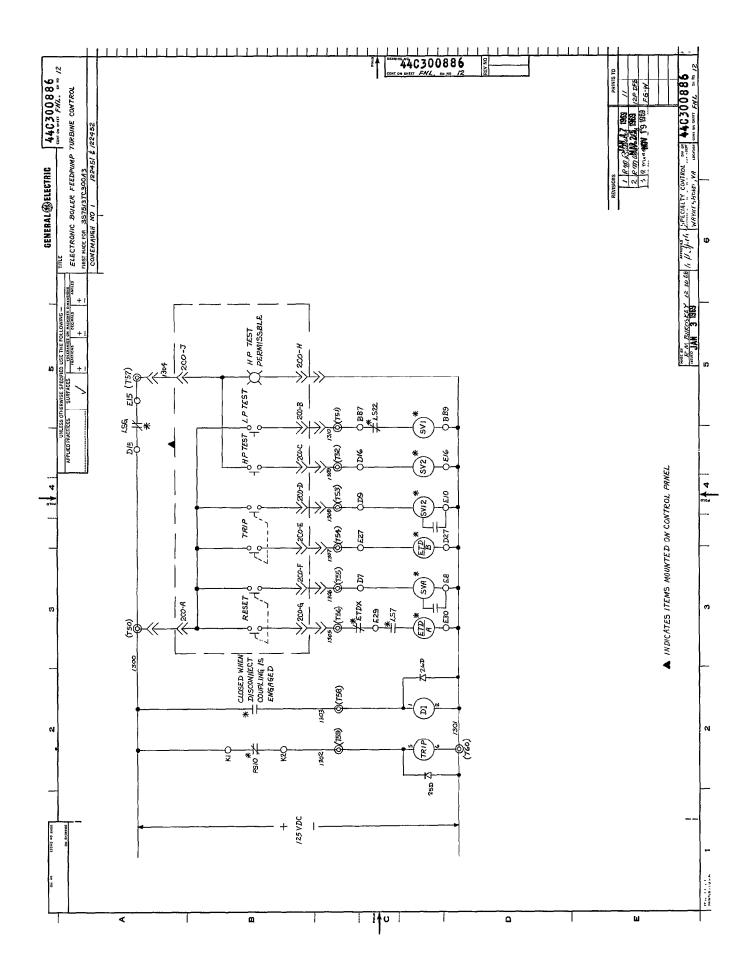


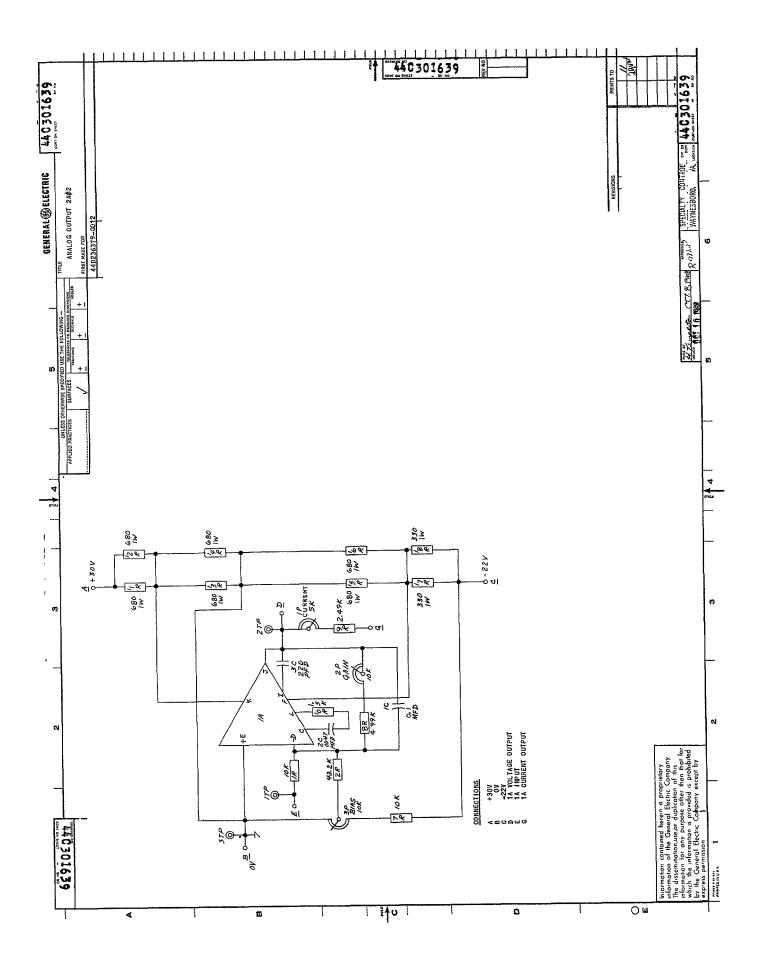


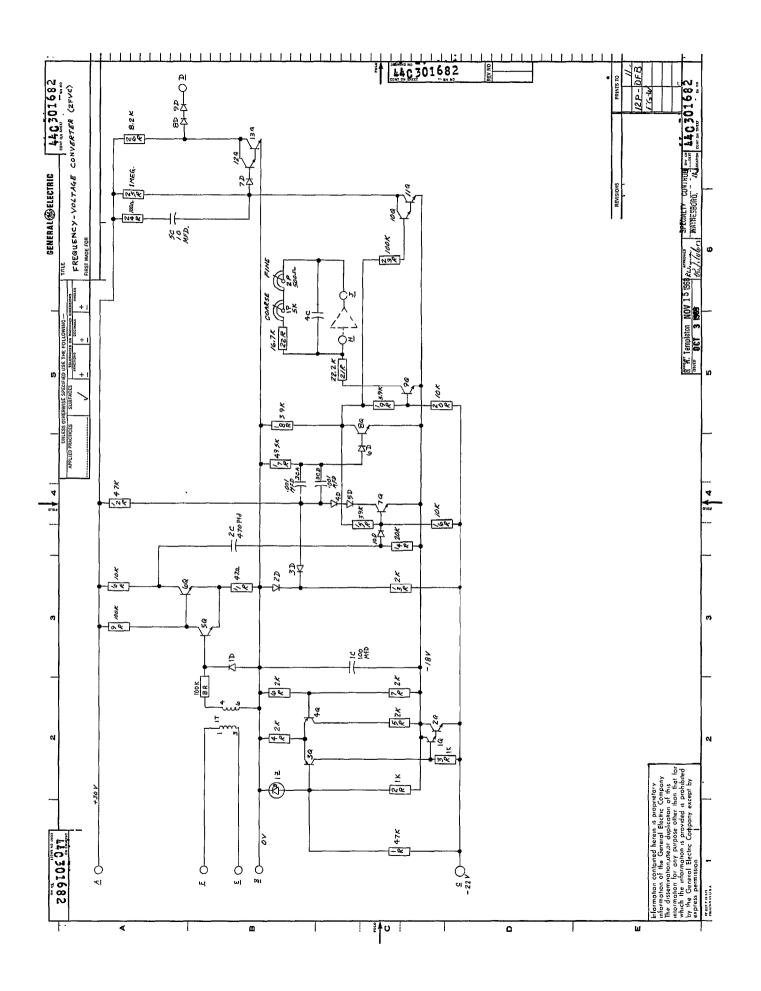


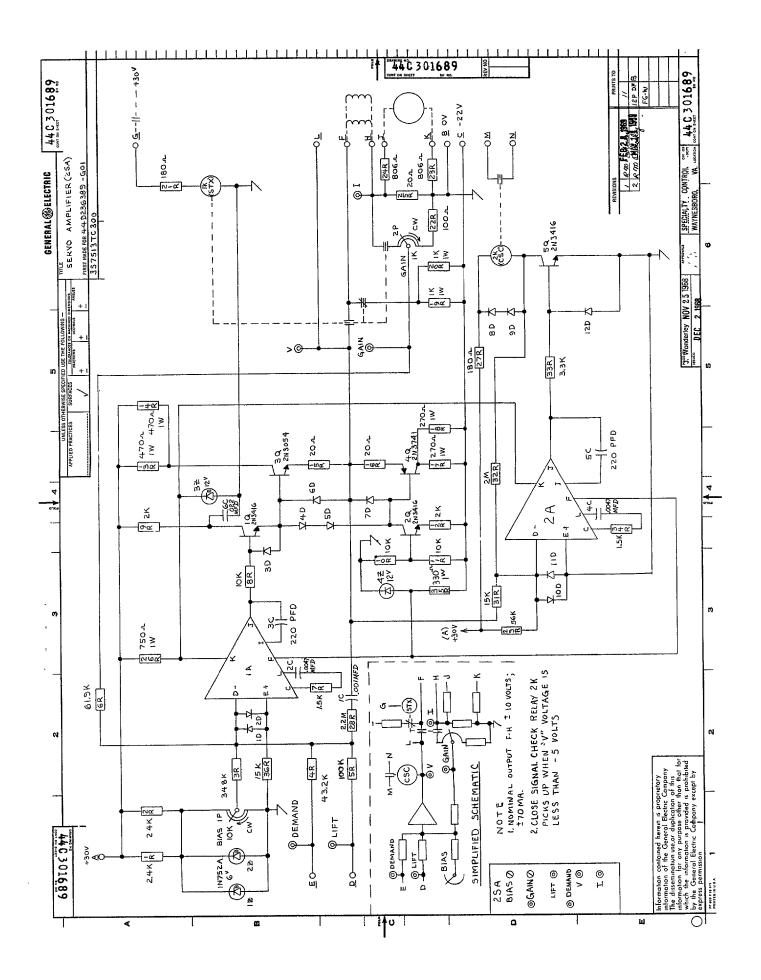


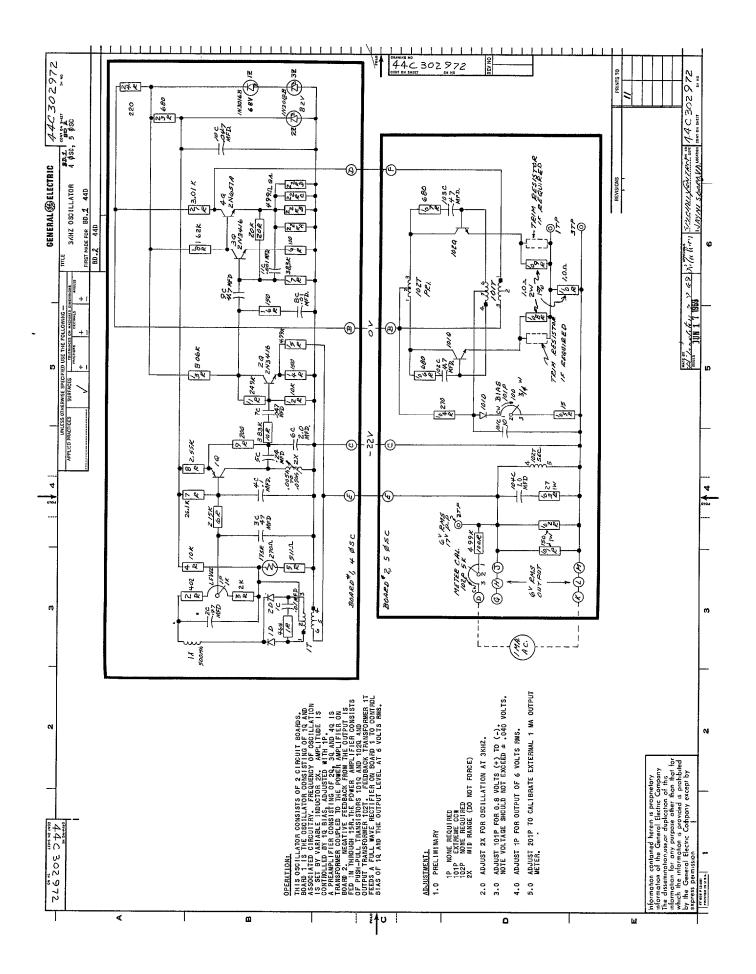


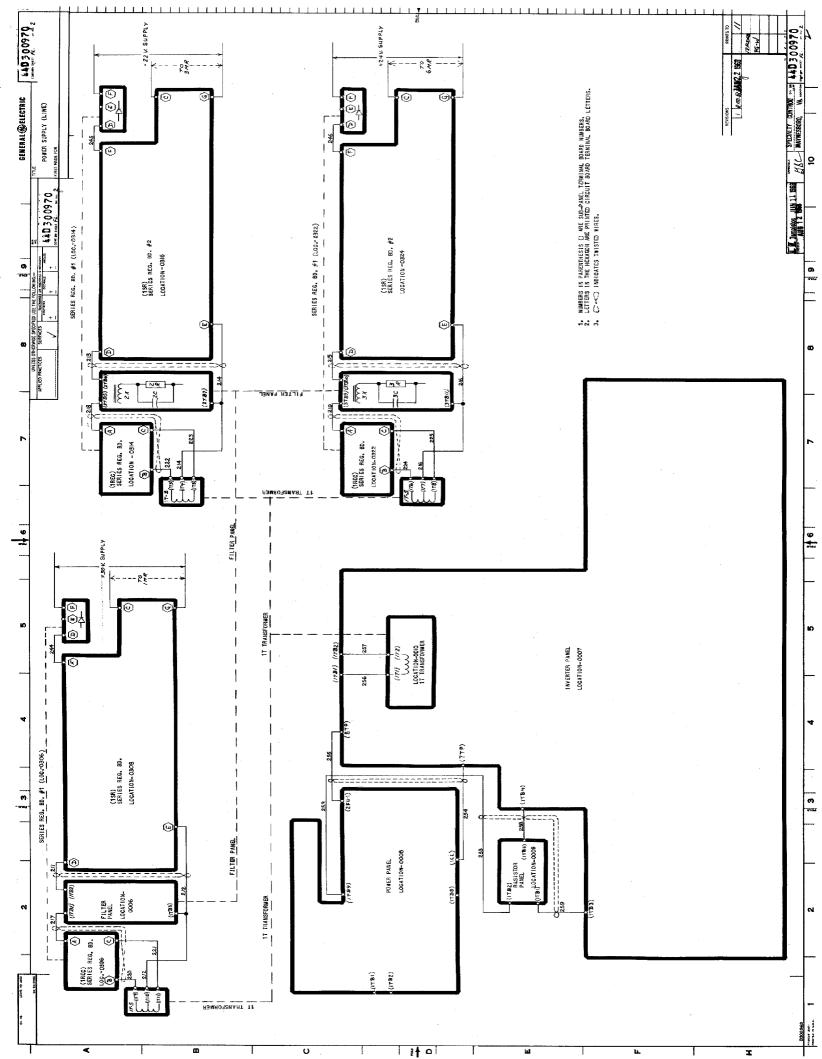


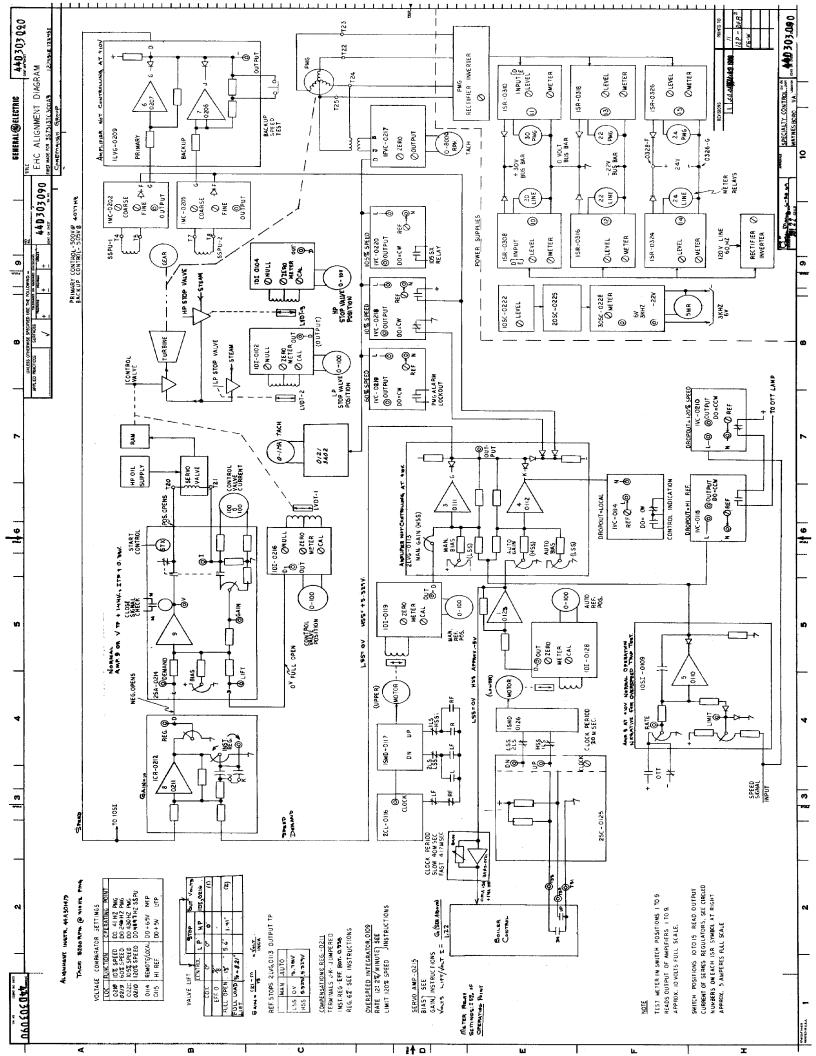


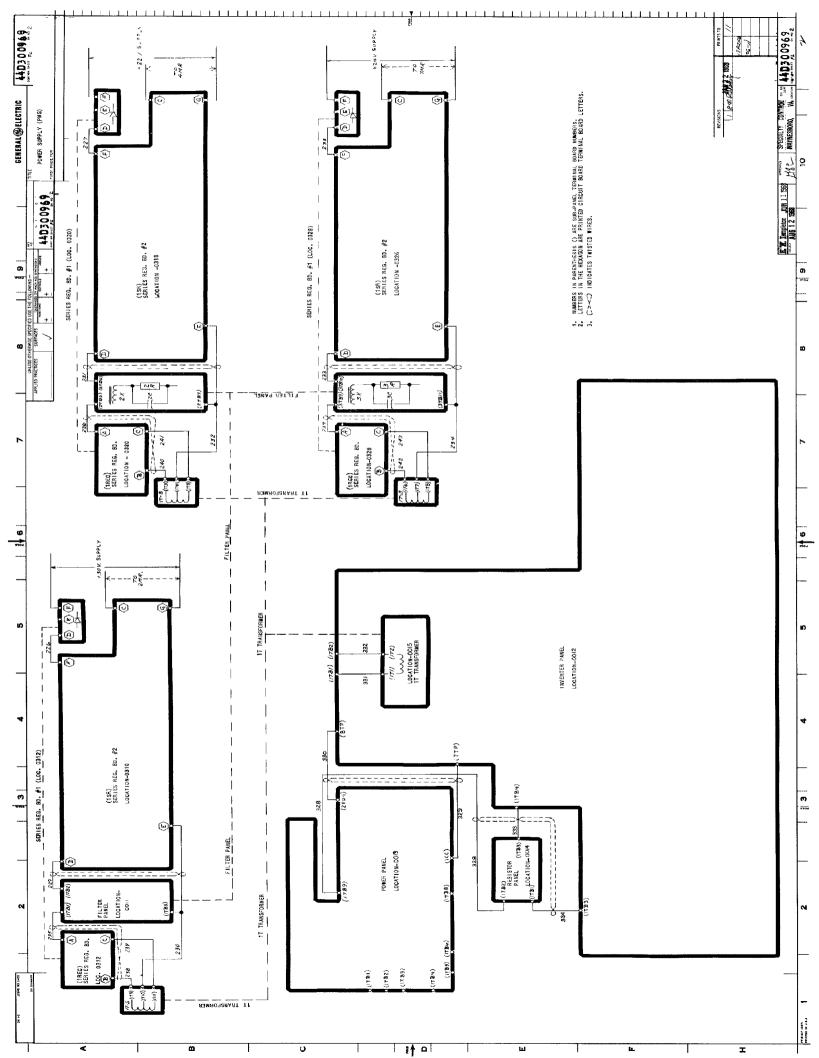


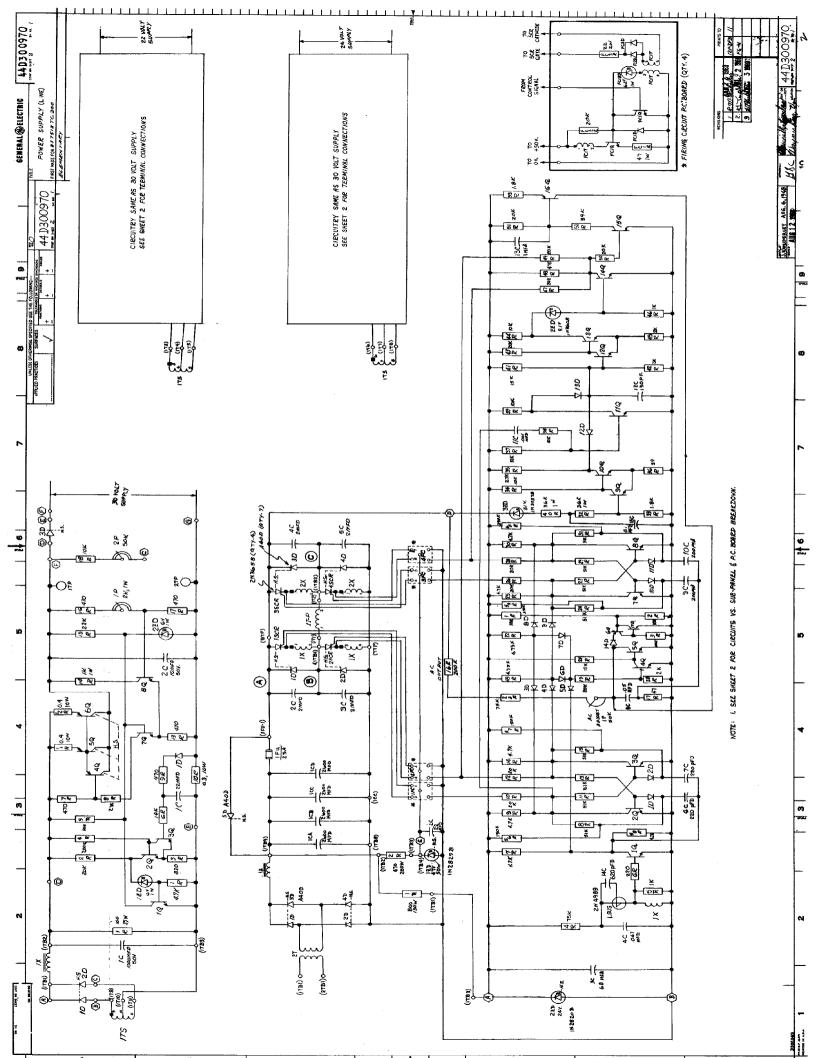


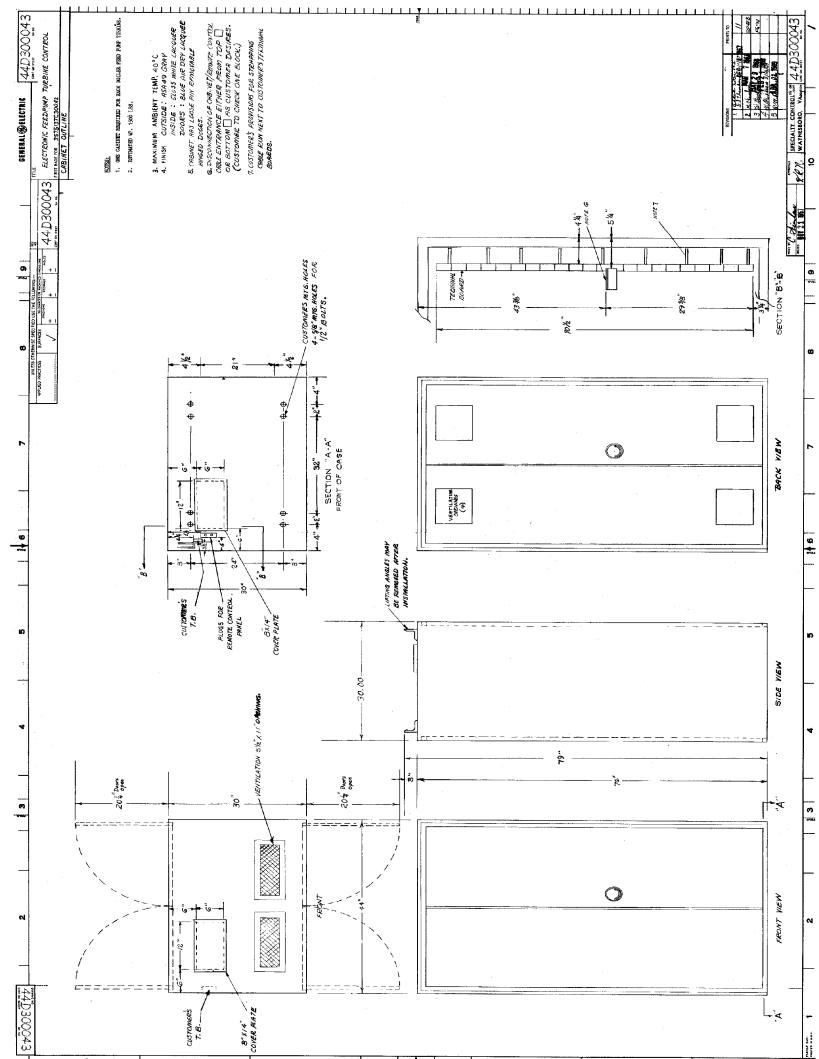


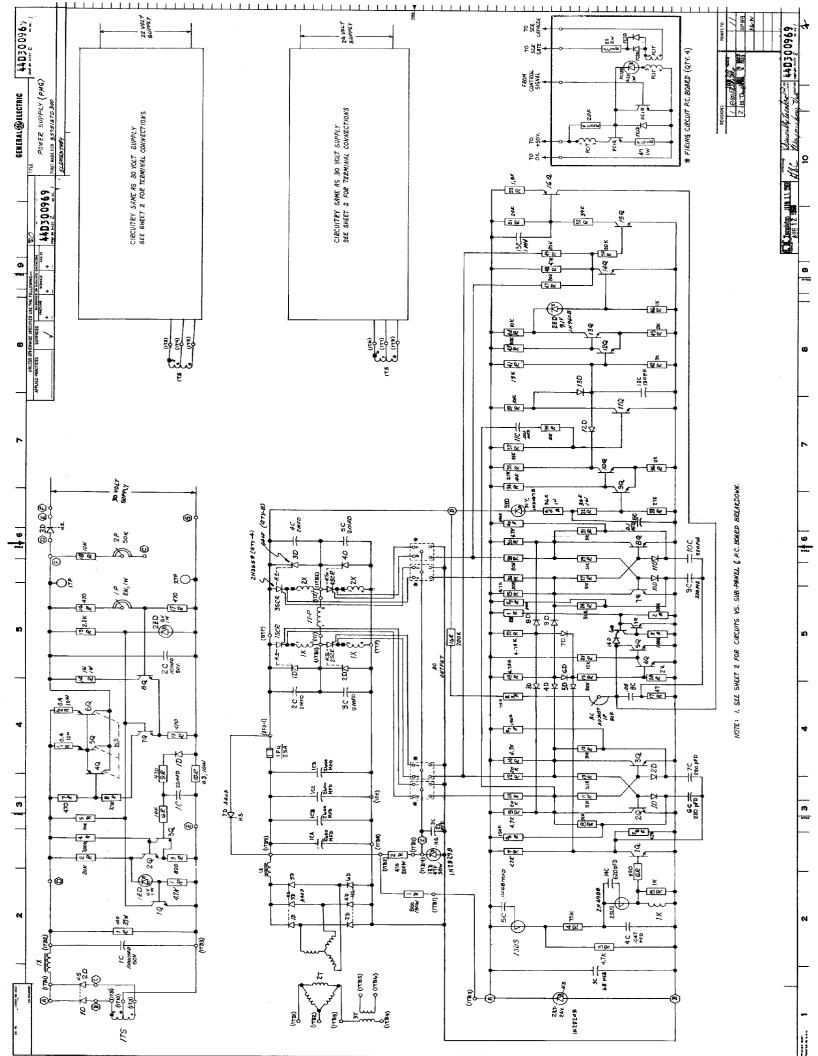












COMMUNICATION AND CONTROL DEVICES DEPARTMENT



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