INSTRUCTIONS

## INSTALLATION - OPERATION - MAINTENANCE


(Photo MG-5568-3)

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## GENERAL (36) ELECTRIC

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## INTRODUCTION

This mstruction book contams helpful suggestions for plaring the Maxspeed Crane Drive equipment in service. It contans general information about drive operation and maintenance.

The operator and maintenance man should have access to a copy of this instruction book.

Additional instructions are included in the supplementary instruction publications and diagrams included in the instruction folder with the equipment.

## RECEIVING, HANDLING AND STORAGE

## RECEIVING

The equipment should be placed under adequate cover immediately upon receipt as packing cases are not suitable for out-door or unprotected storage. Each shipment should be carefully examined upon arrival and checked with the parking list. Any shortage or damage should be reported promptly to the carrier. If required, assistance may be requested from General Electric Company Speed Varıator Products Operation, Erie, PA. When seekıng assistance, please use requisition number and model number to identify the equipment. Telephone $814-455-3219$.

## HANDLING

Wall mounted power units can be transported by lift trucks with the forks completely under the base using care that the unit does not tip.

Floor mounted power units have lifting lugs or holes for litting hars so that crane hooks may be used to pıck up the unit. Spreader bars should be used as required.

## STORAGE

If the equipment is not to be installed immediately, it should be stored in a clean, dry location at ambient temperatures from $-20^{\circ} \mathrm{C}\left(-4^{\circ} \mathrm{F}\right)$ to $+55^{\circ} \mathrm{C}\left(131^{\circ} \mathrm{F}\right)$. The surrounding air must be free of chemical and electrically conductive or corrosive contaminants.

Precautions should be taken to prevent condensation from forming within the equipment enclosure. If the storage environment exceeds a $15^{\circ} \mathrm{C}\left(27^{\circ} \mathrm{F}\right)$ drop in temperature at $50 \%$ humudity over a 4 -hour period, a space heater should be installed inside each enclosure to prevent condensation.
(A 100 watt lamp can sometımes serve as a substitute source of heat). Higher humidities with smaller temperature changes will also cause condensation.

Condensation occurs when arr containıng some moisture is cooled below its dew point. The dew point represents saturation of the air, and is the temperature at which the moisture starts to condense into water. It is not a fixed temperature but rather is related to the mitial temperature of the air and its relative humidity at that temper ature. The amount of moisture that can be held in the arr is related to the air temperature. The following examples illustrate some of these relationships.

TABLE I
Relationship Between Air Temperature, Relative Humidity and Dew Point

| $\begin{gathered} \text { AIR } \\ \text { TEMP } \\ { }^{\circ} \mathrm{F} \end{gathered}$ | ${ }^{\circ} \mathrm{C}$ | RELATIVE <br> HUMIDITY <br> $\%$ | WGT OFMOISTURE <br> IN I LB OF DRY AIR GR INS | DE POIN ${ }^{\circ} \mathrm{F}$ | VT ${ }^{\circ} \mathrm{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 104 | 40 | 100 | 345 | 104 | 40 |
| 104 | 40 | 80 | 270 | 97 | 36 |
| 104 | 40 | 40 | 130 | 75 | 24 |
| 104 | 40 | 10 | 32 | 37 | 3 |
| 50 | 10 | 100 | 54 | 50 | 10 |
| 50 | 10 | 80 | 42 | 43 | 6 |
| 50 | 10 | 40 | $2]$ | 25 | 4 |

In industrial drives, condensation is a possibility in applications where air temperature changes are large and rapid and/or the air is mosst. For example, an outdoor crane operating in sunshine on a winter day, which then is shut down and parked in the shade will experience a rapid drop in temperature. This can result in condensation inside the equipment. Adding heat to keep the air temperature above its dew point can prevent condenヶation.

If storage temperatures below $-20^{\circ} \mathrm{C}\left(-4^{\circ} \mathrm{F}\right)$ are likely to be present then auxiliary heat should he added in each enclosure to maintain temperature at or ahove $-20^{\circ} \mathrm{C}$. For assıstance in heater size selection contact General Electrıc Company.

When a drive that has been in operation is shut down for either a short or extended period of time, it is recommended the environmental conditions be maintaned the same as when in operation. Power, ventilation or heating and airconditioning (If used) should be left on during the downtme to prevent large changes in lemperalure and possible morsture condensation.

## SAFETY FOR PERSONNEL AND EQUIPMENT

The following paragraphs list some general safety reminders and safety recommendations to be followed when operating or installing this equipment.

## WARNING

DENOTES OPERATING PROCEDURES AND PRACTICES THAT MAY RESULT IN PERSONAL INJURY OR LOSS OF LIFE IF NOT CORRECTLY FOLLOWED.

COLOR - BLACK OR WHITE LETTERING ON RED FIELD.

## CAUTION

DENOTES OPERATING PROCEDURES AND PRACTICES THAT, IF NOT STRICTLY OBSERVED MAY RESULT IN DAMAGE TO, OR DESTRUCTION OF, THE EQUIPMENT.

COLOR - BLACK LETTERING ON AMBER FIELD.

## NOTE

DENOTES AN OPERATING PROCEDURE OR CONDITION WHICH SHOULD BE HIGHLICHTED.

COLOR - BLACK LETTERING ON A WHITE FIELD.

## WARNING

IMPROPER LIFTING PRACTICES CAN CAUSE SERIOUS OR FATAL INJURY.

LIFT ONLY WITH ADEQUATE EQUIPMENT AND TRAINED PERSONNEL.

## WARNING: HIGH VOLTAGE

ELECTRIC SHOCK CAN CAUSE PERSONAL INJURY OR LOSS OF LIFE. CIRCUIT BREAKERS, IF SUPPLIED AS PART OF THE TOTAL SYSTEM, MAY NOT DISCONNECT ALLPOWER TO THE EQUIPMENT. SEE SYSTEM ELEMENTARY DIAGRAMS. WHETHER THE AC VOLTAGE SUPPLY IS GROUNDED OR NOT, HIGH VOLTAGE TO GROUND WILL BE PRESENT AT MANY POINTS. WHEN INSTRUMENTS SUCH AS OSCILLOSCOPES ARE USED TO WORK ON LIVE EQUIPMENT, GREAT CAUTION MUST BE USED.

WHEN ONE OF THE INSTRUMENT LEADS IS CONNECTED TO THE CASE OR OTHER METAL PART'S OF THE INSTRUMENT, THIS LEAD SHOULD NOT BE CONNECTED TO AN UNGROUNDED PART OF THE SYSTEM UNLESS THE INSTRUMENT IS ISOLATED FROM GROUND AND ITS METAL PARTS TREATED AS LIVE EQUIPMENT. USE OF AN INSTRUMENT HAVING BOTH LEADS ISOLATED FROM THE CASE PERMITS GROUNDING OF THE CASE EVEN WHEN MEASUREMENTS MUST BE MADE BETWEEN TWO LIVE PARTS.

## CAUTION

DO NOT REMOVE PRINTED CIRCUIT CARDS FROM THE EQUIPMENT WHILE POWER IS APPLIEI). THIS CAN DAMAGE THE EQUIPMENT.

## NOTE

ALWAYS READ THE COMPLETE INSTRUCTIONS PRIOR TO APPLYING POWER OR TROUBIESHOOTING THE EQUIPMENT. FOLLOW THE START—UP PROCEDURE STEP BY STEP.

READ AND HEED ALL WARNING, CAUTION AND NOTE LABELS POSTED ON THE EQUIPMEN'T.

## CAUTION

DO NOT REMOVE INPUT POWER FROM THE DRIVE UNTIL IT HAS FULLY EXECUTED A STOP SEQUENCE, AS THIS CAN DAMAGE THE DRIVE SYSTEM.

## INSTALLATION

## LOCATION

DC-SCR drive power units are suitable for most factory areas where other industrial equipment is installed. They should be installed in well-ventilated areas with ambient temperatures ranging from $0^{\circ} \mathrm{C}\left(32^{\circ} \mathrm{F}\right)$ to $40^{\circ} \mathrm{C}:\left(104^{\circ} \mathrm{F}\right)$ and relative humidities up to 90 percent. It should be recognized; however, that since the life expectancy of any electronic component decreases with increased ambient temperature, reduction of the ambient temperature will bring about extended component life. For example, longer component life should be expected if the ambient temperature is held between $20^{\circ} \mathrm{C}\left(68^{\circ} \mathrm{F}^{\prime}\right)$ and $30^{\circ} \mathrm{C} \cdot\left(87^{\circ} \mathrm{F}\right)$.

Proper performance and normal operational life can be expected by maintaining a proper environment for the drive system.

(Photo 116,5230 i)
FIG. 1 VALUTROL POWER UNIT

Environments which include excessive amounts of one or more of the following characteristics should be considered hostile to drive performance and life:

1. Dirt, dust and forergn matter.

2 Vibration and shock.
3. Mossture and vapors.
4. Temperature excursions.

5 Caustic fumes
6. Power line fluctuations.
7. Electromagnetic interference (noise).

Totally enclosed power units should be positioned to permit heat radiation from all surfaces except the bottom; otherwise, the enclosure can be positioned as follows:

A wall mounted power unat enclosure (or floor mounted enclosure) may be placed side by sode with another enclosure. Clearance at least equal to the width of the enclosure should be avatlable in front so that the door may be fully opened for easy access.

## WARNING

SOME POWER UNITS ARE FURNISHED WITH PARTIAL ENCLOSURES OPEN AT TOP AND BOTTOM. THESE ARE INTENDED ONLY FOR MOLNTING IN ANOTHER ENCLOSLIRE OR IN A CONTROL ROOM HAVING ACCESS BY QUALIFIED PERSONNEL ONLY'. EXPLOSIONS OR FIRES MIGHT RESULLT FROM MOUNTING DRIVE POWER UNITS IN HAZARDOLS AREAS SUCH AS LOCATIONS WHERE INFLAMMABLE

OR COMBUSTIBLE VAPORS OR DUSTS ARE PRESENT. DRIVE POWER UNITS SHOULD BE INSTALLED AWAY FROM HAZARDOUS AREAS, EVEN IF USED WITH DC MOTORS SUITABLE FOR USE IN SUCH LOCATIONS.

## MOUNTING

Wall mounted enclosures may be mounted on any firm, reasonably flat, vertıcal surface.

## NOTE

FOUR HOLES (ONE IN EACH REAR CORNER) ARE PROVIDED FOR MOUNTING THE POWER UNIT. THE BOTTOM LEFT HAND MOUNTING HOLE IS COVERED BY A WIRE BUNDLE. TO GAIN ACCESS TO THIS HOLE, PULL ON THE TAIL ATTACHED TO THE HARNESS AND IT WILL POP DOWN OUT OF THE WAY. AFTER THE POWER UNIT HAS BEEN INSTALLED, POP THE HARNESS BACK INTO PLACE.

An optional mounting arrangement is also avalable which consists of two external brackets (one at the top rear and one at the bottom rear of the power unt enclosure). Each bracket is fitted with two mounting holes for external mounting of the wall mounted enclosure.

## CONNECTIONS

All internal electrical connections between components in DC-SCR drive power units are made at the factory of General Electric Company.

Be sure to protect the interior panel mounted components and sub-assemblies from metal particles when cutting or drilling entrances for interconnecting wiring and cables.

If additional relays, contactors, or electrical solenords are added in the proximity of the SCR equipment enclosure, RC suppression networks should be added across the couls. A series combination of a 220 ohm resistor and a 05 mfd capacitor in parallel with the relay coils is recommended for 115 VAC control circuit.

## NOTE

SOME SYSTEM TRANSFORMERS AND OTHER aPPARATUS ARE SHIPPED SEPARATELY AND MUST BE MOUNTED AND CONNECTED TO THE SYSTEM.

## WARNING

ALL MOTOR BASES AND EQUIPMENT ENCLOSURE housings shoutd re connected to the FACTORY OR FACILITY EARTH GROUNDING SYSTEM.

## NOTE

IT IS RECOMMENDED THAT THE DRIVE SYSTEM COMMON CIRCUIT BE GROUNDED AT ONLY ONE POINT. THIS MEANS THAT IF THE DRIVE REFERENCE IS SUPPLIED BY A NUMERICAL CONTROL OR PROCESS INSTRUMENT WITH GROUNDED COMMON, THE DRIVE COMMON SHOULD NOT BE GROUNDED. IF THE SECONDARY OF THE TRANSFORMER MUST BE GROUNDED, IT IS RECOMMENDED THAT HIGH RESISTANCE grounding be used For grounding The TRANSFORMER NEUTRAL.

## CAUTION

INSTALLATION WIRING MUST BE IN ACCORDANCE With the national electrical code and be CONSISTENT WITH ALL LOCAL CODES. SECONDARIES OF 115 VOLT CONTROL TRANSFORMERS TYPICALLY HAVE ONE SIDE FUSED AND THE OTHER GROUNDED OR AVAILABLE FOR GROUNDING BY THE USER.

## CAUTION

MEGGERING CAN DAMAGE ELECTRONIC COMPONENTS. DO NOT MEGGER OR HI-POT WITHOUT CONSULTING THE SPEED VARIATOR PRODUCTS OPERATION, GENERAL ELECTRIC COMPANY.

## CAUTION

DO NOT CONNECT ANY EXTERNAL CIRCUITS OTHER THAN SHOWN ON THE ELEMENTARY DIAGRAM, SUCH AS AMMETERS ON THE SHUNT OR VOLTMETERS ON THE TACHOMETER BECAUSE THE PERFORMANCE OF THE DRIVE SYSTEM MAY BE DEGRADED.

## CAUTION

DO NOT USE POWER FACTOR CORRECTION CAPACITORS WITH THIS EQUIPMENT WITHOUT CONSULTING THE SPEED VARIATOR PRODUCTS operation, general electric company.

## DAMAGE MAY RESULT FROM HIGH VOLTAGES

 generated when capacitors are switched.Before power is applied to the drive system, cherks ahould be made to see that all internal connections are tight, that plug in printed circuit cards in the optional regulator rack are fully seated and that all open relays and contactors. operate freely by hand. Check that the equipment is clean and that no metal chips are present.

## MAINTENANCE

Periodically inspect and maintan the equipment protective devices (particularly ar filters when supplied) per mstructions in this section. Check all electrual connectoons for tightness; look for signs of poor connectoons and over heating (arcing or discoloration)

## FANS AND FILTERS

On force ventilated drives, the power unit contains a fan and perhaps an air filter in the intake of the enclosure and/or on equipment inside the enclosure.

Inspect the fan at regular intervals to see that it is operating properly. Check for excessive noise and vibration, loose fan blades and for over heating of the motors. Keep the fan blades clean.

If the fan does not operate, replace the fan and integral motor with a unit with the same catalog number.

Clean and/or replace arr filter as appropriate depending on the accumulation of dirt for the type supplied.

To clean metal filters, flush only with warm water, dry and recoat lightly with RP® Super Filter Coat or equivalent (light oil) or replace the filter.

Be sure to install filters with air flow direction as mdicated on the filter.

## DC MOTORS

Maintenance instructions covering brushes, commutator and lubrication are in GEK- 2304 which is found elvewhere in the instruction book.

## PRINTED CIRCUIT CARDS

Printed circuit cards normally do not require maintenatme except to keep them clean and tightly secured to their respective terminal boards or tightly plughed in the
optional modification rack receptacles. Clean as follows:

1. Dry Dust - Vacuum clean, then blow with dry filtered compressed air (low pressure supply).
2. Oily Dirt - Certain components (electrolytic capacitors, switches, meters, potentiometers and transformers can be damaged by solvent, so its use is not recommended. If absolutely necessary, use solvent sparingly on a small brush and avoid above components. Clean contact terminals with dry nonlinting eloth after solvent has been used. Recommended solvents: Freon* RE or TF.
3. If the card is badly contaminated or corroded, replace.

## SILICON CONTROLLED RECTIFIERS

Keep SCR's and heatsink free from dirt, oil or grease, since any accumulation of dirt may cause overheating. Clean as follows:

1. Dry Dust - Vacuum clean, then blow with dry, filtered compressed air (low pressure).

## CAUTION

## SOLVENT CAN HARM NON-METAL COMPONENTS.

2. Oil Dirt - Use dry or barely moist (with solvent) non-linting cloth. Repeat until cloth remains clean. All contact tips must be cleaned with dry non-linting cloth after solvent has been used. Recommended solvents: Freon* RE or TF.

## CONTROL DEVICES

Inspect all relays and contactors at regular intervals and keep them free from dirt, oil or grease. Check for freedom of moving parts, corrosion, loose connections, worn or broken parts, charred insulation or odor, proper contact pressure and remaining wear allowance on contacts. Do not lubricate the contacts as lubrication shortens their life.

Both copper and silver contacts will become darkened and somewhat roughened in normal operation. This does not interfere with their performance, and does not indicate that the contacts should be filed. In general, contacts will not need attention during their normal life, but if prominent beads form on the surfaces due to severe arcing, the contact faces may be dressed with a fine file. Do not use sand paper or emery cloth.

Any contact that is worn to the point where contact wipe or pressure is lost should be replaced. Contactor shunts which are badly frayed or broken should also be replaced.

Cleaning procedure is the same as previously given for SCR and heatsink.
*Trademark of E. I. DuPont Company.

TYPICAL ELEMENTARY


STANDARD CAB CONTROLLED
HOIST DRIVE SYSTEM

## INSTRUCTION INFORMATION

The instruction folder furmshed with the equipment meludes detailed instructions and diagrams applicable for each specific drive system.

In addition to this general instruction, the folder includes mstruction for the motor(s) and other components furmshed. Start-up and troubleshooting gurdes are moluded. All instructions and the accompanying diagrams should be consulted before applying power to the system.

## THE FOLLOWING INFORMATION IS OF PARTICULAR IMPORTANCE.

## TYPES OF DIAGRAMS

Different types of control diagrams are provided for specific purposes. The type of control diagram is noted in the title block of each diagram sheet.

The two major types of diagrams are Elementary, (sometimes called schematic) and Layout or Connection

The Elementary diagrams represent (in symbolic form) the fundamental operation and relationship of the elertrical parts of a system. These diagrams are drawn so that the operation of the control system can be easily understood. Connections made between control devices and power devices within the enclosure are also shown in this type of dagram.

The Layout or Connection diagram, when supplied is onte which shows the relative physical position of the devices as well as other electrical components located within the came enclosure.

The Elementary diagram also identifies adjustments, ugnals and test points In this instruction book, adjusiments are in special type. Example: FMAX (Maximum motor field adjustment).

Signals and test points are CAPITALIZED. Example: CFB (Current Feed back)

## PRINCIPLES OF OPERATION

## maxspeed crane drive description

The Maxspeed Crane Drive System is a D-C adjustable-
voltage drive operating from an A C power source The basic drive consists of a D.C shunt wound motor, an SCR power conversion module operating on A.C power and supplying adjustable voltage D-C power to the D-C motor, an A-C/D-C control panel and a masterswitch or pendant station for controlling direction of rotation and speed. In addition, the drive includes provision for a brake, normally magnetic shunt wound and spring-set, and limit switches. The control panel is furnished as a packaged unit complete with internal wiring and interconnections, plus terminals for external power and control leads The enclosure doors are removable for increased accesubility. See Fig. 2 for simplified crane drive elementary diagram.

The Maxspeed Drive is a speed control drive providing programmed speed versus load characteristics and smooth acceleration and deceleration regardless of how rapidly the operator manipulates the controller. The Maxspeed Drive "number" refers to the programmed speed characteristic selected for the drive and is the percent of full load hoist speed at which the drive will operate in the hoisting direction at no-load. For example, the no-load hoisting speed of a Maxspeed 250 is 250 percent of full load hoist speed.

In the Maxspeed Drive no armature loop or field reversing contactors are required because reversing is accomplished statically. The motor armature is controlled by a 3 -phase static reversing phase-controlled rectifier, and the motor field is controlled by a static unidirectional phasecontrolled rectifier.

To stop from a fast speed, the Maxspeed Drive decelerates the motor by regenerative braking before the mechanical brake is set. This saves wear on the brake and lessens the strain on the machinery.

The Maxspeed 100 Drive is a regulated speed control drive using the inherent characteristics of a shunt wound motor. The maximum no-load hoisting speed is approximately the same as full-load horsting speed (See Fig. 3) with the armature voltage being regulated. 'The throw of the master switch determines the direction and speed. Since the maximum speed is rated speed, no field weakening is required, therefore, there may be no motor field programmer in the Maxspeed 100, and the D-C motor field may be connected to a static exciter. The lowering speeds are approximately those shown in Fig. 3.

The Maxspeed 175, 250, and 320 Drives are common speed versus load characteristics (See Fig. 3); however, mtermediate characteristics are provided to meet various applications. The curves on Fig. 3 show the range of speeds from minımum throw of the masterswitch to full throw for


FIG. 3 TYPICAL SPEED-LOAD CURVES FOR MAXSPEED HOIST DRIVES
rach characteristıc where speed is a function of hook load. The particular characteristic selected for a drive is determined by the application requirements and the rapability of the DC motor. How this characteristic is set up in the regulator is covered in later sections.

## GENERAL DESCRIPTION

The basic elements of a typical VALUTROL Maxspeed Drive System are shown in the simplified typical block diagram, Fig. 4.

I'hree-phase $A C$ power enters through the primary winding of a separately mounted isolation transformer. Since this drive employs three-phase, half-wave rectification of $A C$ power, the transformer must have a secondary neutral connection (XO).

Power is fed through the circuit breaker and the MA contactor and enters the power conversion module (SCR) where it is converted to DC adjustable voltage. DC current is fed through a shunt to the DC motor armature. The return side of the DC motor is connected to the isolation transformer neutral connection (XO).

The speed of the motor is proportional to the DC voltage applied to its armature.

The basic control is manufactured on five (5) removable printed circuit boards. These are the power supply card (PSC), the main control card (MCC), the interface card (IFC), the motor field control card (MFC) and the diagnostic card (DGC).

Custom features of the Maxspeed Drive are found in the modification rack. These features include a reference card (REF) and a torque proving card (TQP). If motor field programming is required, host and lower programming cards (HPC and LPC) are provided. The brake permissive relay ( BPR ) provides a pilot signal to the brake contactor.

The three-phase mput also supplies power to the motor held control (MFC) and to the control power transformer. (CPT) This transformer is fitted with a $460 / 230 \mathrm{~V}$ weconnectable primary winding and two isolated secondary windings: (1) 115 V to operate the coll of the MA contactor and conversion module cooling fans, and (2) the second winding is a 50 volt center tapped secondary which provides $A C$ input to the power supply card.

## MAIN CONTROL CARD (MCC)

The primary purpose of the main control card is to drive the conversion module (SCR) as commanded by the specd reference and feedback signals.

This card also performs several additional functions such as linear timing of the reference; current limit; "Ready to Run" indicator and various scaling and trimming adjustments.

A total of eleven (ll) potentiometers are provided on this card, ten (10) of which are accessible from the front of the controller. The eleventh potentiometer, the card zero adjustment ZERO ADJ, is preset at the factory and should normally not be disturbed. The ten accessible potentiometers are:

| DAMP | MAX SPEED | MIN SPEED |
| :--- | :---: | ---: |
| CUR IIMIT | GAIN | REF SCALE |
| CEMF LIMIT | RESPONSE | IIN TIME | COMP

## TEST INSTRUMENT AND PROBE

Located below the man control card (to the left) is a test instrument and probe that can be used to read out signals from any of the drive test points. The probe is fitted with two connections, one for the 4 volt instrument scale and the other for the 20 volt scale. Always apply the 20 volt connection first. If the reading is below 4 volts, switch to the 4 volt connection for improved accuracy of the read out.


(Photo M(, 5236 17)

## INTERFACE CARD (IFC)

The primary purposes of the interface card are:

1. To provide low level isolated signals corresponding to the three-phase AC, DC armature voltage, armature current and tachometer feedback.
2. To control the start, stop and synchronizing of the drive while monitoring the system for abnormal operating conditions.
3. To provide one milliampere signals for external speed and current indication.

Other outputs provide:

1. A NO/NC contact indicating MA closure (MAX).
2. A NO contact indicating a fault condition (FLT).

There are (5) putentiometers on this card.

1. The IZERO is a bias adjustment for the current feedback output and is factory set. This control should not be disturbed.
2. ICAL is the calibration adjustment for CFB and is factory set. This control should not be disturbed.
3. $R S T O P$ is the drop out level of the regenerative stop sequencing circuit and is also factory set.
4. IMET is the callbration adjustment for the current indicator.
5. SMET is the calibration adjustment for the speed indicator.

Adjustment 4 and 5 will be factory set if the indicators are ordered with the drive and mounted in the power unit enclosure.


## FIG. 6 INTERFACE CARD

## MOTOR FIELD CONTROL CARD (MFC)

This card provides a current regulated motor field supply for the DC motor. Constant field excitation is supplied for Maxspeed 100 Drives. On Maxspeed Drives where field programming is required, the current reference is modified by the hoist and lower programming card to achieve the desired speed versus load characteristic.

The tachometer monitor circuit is used to monitor SFB and detect an overvoltage. Loss of motor field is also detected by this card. Any of these faults will shut down the drive. A field economy circuit is also included on this card, which automatically reduces the level of motor field excitation whenever the drive is shut down, thereby avoiding the possibility of excessive temperature (at stand still) and/or reduced insulation life. See GEK-24971 for detailed instructions.

(Photo MG-5236-15)
FIG. 7 MOTOR FIELD CONTROL CARD

## DIAGNOSTIC CARD (DGC)

The diagnostic card performs no function under normal operating conditions but will program the drive into a diagnostic run mode and diagnostic static mode for ease in initial start up and troubleshooting.

## POWER SUPPLY CARD (PSC)

The power supply card rectifies the AC input and provides regulated plus and minus 20 volts for the printed circuit cards. Unregulated plus and minus 30 volts DC is also provided to drive the static logic switches and the MAX relay. All of the DC outputs are fused to protect the power supply card against overloads. The regulated plus and minus 20V DC outputs are protected against over voltage conditions caused by a power supply card failure.


FIG. 8 POWER SUPPLY CARD

(Photo MG-5393-1)
FIG. 9 DIAGNOSTIC CARD AND MODIFICATION RACK

## CONTROL FUSES, MOV'S

The signal power for the control is taken from the threephase input through control fuses to the control voltage transformer. The control fuses are used to protect the control transformer and the metal oxide varistors (MOV) which are used to protect the power unit from excessive transient over voltage conditions. Three (3) high resistance wires which provide line synchronization are connected to the load side of these fuses. The drive will not operate if any one of these fuses is open.

## POWER CONNECTIONS

The power connections are the three-phase input at LlA, L2A, and L3A on the circuit breaker; the transformer neutral at XO ; motor field at Fl and F 2 on the ATB terminal board and the DC power output DAI.

## SIGNAL CONNECTIONS

All signal connections are made on the $2 \mathrm{~TB}, 3 \mathrm{~TB}$ and 4 TB terminal boards and their functions are described in Table II.

## MODIFICATION RACK (MDR)

Provided on printed circuit cards located in the modification rack below the main control card are the special features and functions of the Maxspeed Drive These features include:

Operational check.
Provision for induction masterswitch.
Torque proving.
Slowdown or spotting control.
Hoist motor field programmıng.
See Modification Features for details of these functions. Other special functions such as stepped reference or independent timed acceleration and deceleration adjustments may also be added.


TABLE II SIGNAL CONNECTIONS

| 2 TB NO | NOMENCLATURE | DESCRIPTION |
| :---: | :---: | :---: |
| 1 | $-30 \mathrm{~V}$ | Unregulated negative DC voltage used as the return line for the CONTOL ON function and the static switches RUN and JOG, and possible modifications. |
| 2 | CONTROL ON | If CONTROL ON is not connected to - 30 V the drive will not start. If CONTROL ON is opened with the drive operating, the contactor will open and the drive will coat. |
| 3, 4 | FLT | A normally open, held closed relay contact. L $n d e r$ normal conditions this contact is closed. If a fault condition is detected, this contact opens. Usually ronnected to the undervoltage circuit to remove control power. |
| $5,6,7$ | MAX | A NO/NC relay contact which actuates when the contactor actuates. |
| 8, 27 | COM | Signal common. All signals are measured with respect to common, unless otherwise noted. |
| 9 | EST | External Fault Stop input. If EST is momentarily disconnected from common, the contactor will open and the motor will coast. The drive may not be restarted until the reset line is momentarily connected to COMMON (2TB-12). (Sce RESET below). |
| 10, 11 | FX1, X2 | The internal 115 V AC. FX1 is fused for external use. |
| 12 | RSET | Reset inpur. All fault shut downs inhihit the drive from starting until the fault has been cleared and the drive in reset. After the motor has come to a stop, the drive may be reset by momentarily connecting RSET to common. The drive will not restart until RSET is released from common. Momentarily connecting RSET to common or pushing the RESET BUTTON will intiate a coast stop shutdown. |
| $\begin{aligned} & 13,15 \\ & 16,17 \\ & 18,19 \\ & 24,25 \end{aligned}$ | SPl to SP8 | These are special purpose wires which are used to bring additional signals out of 2 TB . Refer to the system elementary for detals. Additional SP wires may be connected to 3 TB and 4 TB as required. |
| 14 | RUN | The drive will not start unless ether RUN or JOG; are connected to -30 V , either at 2 TB or by special purpose logic in the MDR. When RUN and JOG; are released from -30 V , the drive will decelerate to a stop and open the MA contactor. |

TABLE II SIGNAL CONNECTIONS (continued)

| 2 TB NO . | NOMENCLATURE | DESCRIPTION |
| :---: | :---: | :---: |
| 20, 21 | $+20 \mathrm{~V},-20 \mathrm{~V}$ | Regulated power supply outputs. |
| 22 | IMET | Output to an optional lma load instrument. The instrument is calibrated with the IMET potentiometer on the Interface Card. IMET is an absolute (-) signal. |
| 23 | SMET | Output to a lma speed instrument. The instrument is calibrated with the SMET potentiometer on the Interface Card. SMET is an absolute ( - ) signal. |
| 26 | SMIN | Output from the MIN SPEED potentiometer on the main control card. |
| 28 | SR | Speed Reference input. |
| 29,30 | TKP, TKN | Input connections for motor mounted tachometer or machine mounted tachometer. <br> NOTE: WITH A DC TACHOMETER, TKP MUST BE POSITIVE WHEN SYSTEM REFERENCE IS NEGATIVE AND DAl IS POSITIVE WITH RESPECT TO DA2. |


| 3 TB | NOMENCLATURE | DESCRIPTION |
| :---: | :---: | :---: |
| 1 | RLA | Input to time delay relay card (TDR) for relay RLA. |
| 2 | RA | Input to logic relay RA used for run. |
| $6,7,8$ | BPR | A NO/NC relay contact which actuates when the brake permissive relay actuates. BPR responds to a signal from the torque proving card. |
| 4TB | NOMENCLATURE | DESCRIPTION |
| I | RUN | Run signal which is time delayed after normal stop and is connected to the CONTROL ON input through a UV contact. |
| 2 | NSW | Negatıve switch input to reference card to enable negatıve reference. |
| 3 | PSW | Positive switch input to reference card to enable positive reference. |
| $\begin{aligned} & 7,9,10,11 \\ & 12,13,14 \end{aligned}$ | SP37, SP39 to SP44 | Special purpose wires for additıonal signals. |
| 15 | +30V | Unregulated positive DC voltage for reference card input switches. |

## START-UP

The VALUTROL Maxspeed Drive is factory tested with the complete drive system. It is ready to operate provided the external power and control connections have been properly made and the following step-by-step procedures arc followed:

1. Verify that the terminal board screws are tight.
2. Verify that incoming power is the proper voltage and the incoming wiring is complete and correct.
3. Set the diagnostic switch to its NORMAL (center) position. Apply power to the drive. If the green "Ready to Run" light located on the lower left hand corner of the main control card (MCC) is not illuminated, press and release the RESLIT pushbutton on the panel below. If the light does not turn on, the most probable cause is incorrect incoming phase rotation. Remove power, reverse any two of the incoming $A C$ power leads and repeat.
4. Verify that the reference voltage, SR , from $2 \mathrm{~TB}(28)$ to $2 \mathrm{~TB}(27)$ is variable with the external speed adjust controller. (SR must be negative in the hoist or forward direction).

When an induction masterswitch is used, the reference polarity may be changed by interchanging wires on terminals X1 and X3 and on X2 and X4 on the masterswitch terminal board.
5. Slowly move the master controller until the motor starts to rotate. Check motor rotation. If incorrect, remove power and interchange the motor field leads F1 and F2 on ATB terminal board.
6. Run the drive from the external speed reference up to top speed. Adjust MAX SPEED as may be required to set the maximum armature voltage.

If field programming is used, adjust MFH on the hoist card for the no-load hoisting speed, and MFL, also on the horst card, for the no-load lowering speed. The value of FC at the top no-load speeds should be recorded for future reference. DO NOT OVERSPEED.
7. Close and secure the doors of the power unit

## WARNING

BEFORE LIFTING A LOAD, THE BRAKE LININOS SHOULD BE "WORN IN" SUFFICIENTLYY PER THE MANUFACTURER'S INSTRICTIONS

## TABLE III FAULT CONDITIONS

A fault has occurred if the fault relay contact (FLT) is open or if the "READY TO RUN" light is off. The conditions that ran intiate a fault are as follows:

1. No three-phase power.
2. Loss of an incoming phase.
3. Incorrect phase rotation.
4. Al: power fuse blown, or circuit breaker is open.
5. Control fuse is open.
6. Power supply plus or minus $D C$ fuse is open.
** 7. Instantaneous overcurrent (IOC) level exceeded.
7. Motor thermo-switch (MTHSW). (If connected to fault eircuitry).

* 9. Timed overcurrent (TOC) - electronic. (If connected to fault circuitry).
** 10. Loss of motor field. (FF)

11. External Fault Stop momentarily released from Common.

* 12. Other sperial functions to System Trip (SYS) or External Fault Stop inputs.

13. System Trip input (SYS) momentarily connected to +10 volts.
14. RESET button depressed or RESET input momentarily connected to Common with motor rotating.
15. RESET button held depressed or RSET input held connected to Common.
16. Diagnostic mode selected with the motor rotating.
17. Oscillator (OSC) failed - "on."
*18. Tachometer fault (loss of tachometer signal). (If tachometer is used). (TF)
** 19. Overspeed. (Overvoltage indication on reference card).
18. Operatıonal Check (OCK). (Indication on reference card).

* May not be provided. Refer to instructions on Motor Field Supply and System elementary diagram.
** Can be caused by LOC REF and CUR REF settings in Statıc Diagnostic mode.
Atter the fault condtion has been cleared and the motor has come to standstill, the drive can be RESET by any of the following three methods:

1. Momentanly remove the three-phase power and re-apply.
\# 2. Push the RESET button.
\# 3. Momentarily connect RSET to common.
\# If all fault conditions have been cleared but the drive fails to RESET, the RSTOP adjustment may be set too low.
MAXSPEED
CRANE DRIVE TEST DATA (ALL DATA $\pm 5 \%$, EXCEPT WHERE NOTED)


## SEQUENCE OF OPERATION

## POWER APPLIED

The control trancormer (CPT) is energized through its prumary fuses. The fans (if supplied) will come on.

The power supply card is energized and the DCoutput ( $\pm 20$ volt) are applied through their fuses to the rest of the cards. All readings carry a tolerance of $\pm 10 \%$.

The motor field supply is energized. Refer to the motor field supply instructions for details.

If no faults have been detected by the monitor section of the interface card, the fault relay FLT will close, and the "Ready to Run" indicator on the main control card will Illuminate. Table III tabulates the fault conditions which are monitored.

The oscollator will start, and the synchronizing signals SA, SB, SC will measure 8.5 volts RMS, ( $\pm 10 \%$ ). See Figure 19.

## SWITCH LOGIC

RUN will be switched from +30 V to -30 volts by an RA contact which is a function of the run permissive relay and masterswitch. The control line MAC from the main control card to the interface will be pulled down to -20 volts.

The interface card checks that no faults exist and that "control on" is connected to -30 volts before applying power to the coil of the pilot relay MAX.

MAX preks up, releasing the preconditioning signal PRE from common and applies power to the coll of the MA contactor.

When PRE is released from common, it switches to -4 volt, which will release the main control card preconditioning after approxımately 80 milliseconds.

Releasing preconditioning allows the drive to send firing puises to the gates of the SCR's in the conversion module, and allows the normal signal flow to occur.

## SIGNAL FLOW

If RUN 19 switched, the reference at SR is applied to the linear tume section The timed reference output TR will lamp to a voltage proportional to SR. The MAX NEG or

the masterswitch is set for top speed. The time for TR to ramp from 0 to 10 volts is adjustable from .3 to 60 seconds with the LIN TIME adjustment. See jumper table on system elementary. (Ranges: . 3 to 7 sec . or 2 to 60 sec .).

The VFB feedback from the motor is isolated with a resistor network in the feedback harness. VFB is connected to the system feedback. The output of the system feedback section is SFB, and will be 10 volts at top voltage. MAX SPEED is adjusted to make the actual top voltage correspond to desired top voltage.

The timed reference TR, and the system feedback SFB are summed by the regulator error amplifier. The error amplifier output EAO will be a low voltage (nearly zero) when the drive is regulating voltage. EAO will not be low when the drive is in current limit or CEMF limit. The gain of the error amplifier is set with the GAIN adjustment. The GAIN adjustment is used primarily to improve the response of the drive in the constant horsepower region when the motor field supply is a motor field control MFC.

To manntan good load regulation, the error amplifier is fed into the regulator integrator. The output of the integrator is the reference, $D R$, to the driver. The response of the control below base speed is set with the RESPONSE adjustment.

There is a limit, however, to how responsive a drive may be set. Stability of the drive is decreased as its response is increased. The RESPONSE adjustment is desensitized when the drive is operating in the constant horsepower region of the torque speed curve by the WFR signal from the motor field control (MFC).

To protect the system, two limit sectıons are provided; counter EMF (CEMF) limit and current limit. The output of the CEMF limit and the current limit drive the regulator integrator and will override the error amplifier, if required. The current hmit is set with the CUR LIMIT adjustment and the counter EMF himi with the CEMF LIMIT adjustment. Typically, the regulator current limit is set at $150 \%$ of the motor nameplate current or 3.75 volts ( $\pm 10 \%$ ) of current feedback, CFB. The counter EMF is normally limited to 250 armature volts at no load, or 5.75 volts ( $\pm 10 \%$ ) of CEMF.

## WAVEFORMS

All illustrations were photographed in the forward motoring quadrant with zero volts on center hime at 2 maer per division.

$2 \mathrm{msec} / \mathrm{div}$
At low current level 1 volt/division
FIG. 12 CURRENT FEEDBACK (CFB)

$2 \mathrm{msec} / \mathrm{div}$
At low current and 100 volts 5 volts/division
FIG. 14 VOLTAGE FEEDBACK (VFB)

$2 \mathrm{msec} / \mathrm{div}$
At contınuous current 1 volt/division
FIG. 13 CURRENT FEEDBACK (CFB)

$2 \mathrm{msec} / \mathrm{d} \mathrm{v}$
At continuous current and 100 volts 5 volts/diviston
FIG. 15 VOLTAGE FEEDBACK (VFB)

## WAVEFORMS

All illuatratıons were photographed in the forward motoring quadrant with zero volts on center line at 2 msec per division.

$2 \mathrm{msec} / \mathrm{div}$
Tvpucal of SA, SB, \& SC
$S B$ laga $5 A$ by $120^{\circ}$
SC. lags SB by $120^{\circ}$
5 volts/division
FIG. 18 SYNCHRONIZING SIGNAL (SA)
$2 \mathrm{msec} /$ div
Normal
1 volt/division
FIG. 19 PULSE OUTPUT (PO)

## WAVEFORMS

All illustrations were photographed in the forward motoring quadrant with zero volts on center lime at 2 mate per divintom

$2 \mathrm{msec} / \mathrm{div}$
With one SCR gate lead open
1 volt/division
FIG. 20 PULSE OUTPUT (PO)

$2 \mathrm{msec} / \mathrm{d} \mathrm{v}$
Gate to Cathode Firing Signal 1C-1C:
Typical of all ux Signals 1 volt/diviston
FIG. 21 GATE TO CATHODE FIRING SIGNAL

The counter EMF signal CEMF is developed on the main control card by subtracting a signal proportional to the IR drop of the motor from voltage feedback. This is set with the COMP adjustment. For most Maxspeed Drives, the COMP adjustment is set so there is no IR compensation. CEMF is then equal to the voltage feedback VFB.

The driver reference, DR, the voltage feedback, VFB, an armature current signal from damping adjustment, DAMP, and the driver current limit output are summed at the input to the driver. The driver converts this error to pulsetrans which drive the SCR gates in such a manner as to maintan the motor voltage proportional to the driver reference. The damping adjustment, DAMP, controls the response of the drıver.

Generally speaking, DAMP, is used only to quiet small oscillations which occur in the current under light load conditions. Too much damping will slow down the system and response and tend to cause over shoot.

The driver provides a signal IPU to the oscillator on the interface card to generate an initial pulse at the exact point in time that an SCR is to be fired. See Fig. 17.

Two driver monitor points are avalable, PCR and PO. PCR is the phase control reference which causes the output pulse trains to phase shift in time with respect to the AC line. As PCR moves from zero to +6 volts $( \pm 10 \%)$, the output pulses will shift from full off to full on. PO is used to monitor the pulse outputs to the SCR's. See Fig. 19.

## STOP

There are two stop sequences, normal stop and fault stop. With a normal stop the drive regenerates to near zero speed before setting the brake and opening the MA contactor. A fault stop sets the brake and opens the MA contactor.

NORMAL, STOP - Move the masterswitch to the OFF position. NSW or PSW on the reference card will open, removing the reference from SR.

The umed reference $T R$ will begin to time down to zero and the drive speed will come down accordingly.

Signal level detector relay SLB will drop out at a low value of CEMF and set the brake to stop the drive. After a time delay, set by run permissive relay RLA, RA drops out removing power from the MAX coll, which in turn drops out MA. The tume delay allows jogging of the drive without dropping out MA and sets the brake in the event SLB does not drop out or the drive does not respond to a stop command.

FAULT STOP - Fault detected (See Table III) or CONTROL ON is open. An emergency stop will imitiate a fault stop sequence by opening CONTROL ON and removing control power

The preconditioning signal PRE is immediately applied to the main control card, forcing the drive into zero current or coast conditions. As soon as the current goes to zero, preconditioning is established throughout the card.

The contactor unconditionally drops out 100 milliseconds after the fault condition occurs. The brake contactor drops out immediately.

The drive cannot be restarted until the motor has come to rest and the masterswitch has been returned to the OFF position.

After the motor has stopped, push the RESET button.

## DIAGNOSTIC STATIC (SWITCH TO LEFT)

## LOGIC

The RUN and JOG inputs are inhibited. This prevents the references SR and JOGR from activating the drive and holds the contactor open.

The current reference potentiometer CUR REF controls the current feedback signal, CFB.

The local reference LOC REF potentiometer is connected into the input of the linear time section and into the system feedback section The local reference is also connected to the field daagnostic reference DFDR. Refer to the motor field programmer description for details of operation.

To simplify signal tracing, the gain of the regulator and drive is reduced and the system feedback signal to the regulator error amplifier is removed.

## SIGNAL FLOW

The local reference LR is apphed directly to the uput of the linear time section, by-passing the REF SCALE adjustment. The timed output TR will ramp to a voltage equal to LR in magnitude and polarity in a time determined by the setting of IIN TIME.

The local reference LR is also apphed to the input of the last stage of the system feedback section. The output SFB will be equal to LR in magnitude, but opposite in polarity. The tachometer scaling circuit and its output TFB are unaffected by the local reference and will remain at zero.

The signal from SFB into the regulator error amplifier is inhibited. The primary purpose of exercising SFB is to check any special function circuits in the modification rack which are programmed from SFB and/or SFB functions of an MFC.

A dummy feedback signal to replace the normal SFB signal is connected from the output of the regulator integrator output DR to the input of the regulator error amplifier. Under these conditions, $D R$ is equal to the magnitude of TR but opposite in polarity as long as the current reference is zero. When the current reference is rased, the current feedback signal CFB will exceed the current limit level set by CUR LIM and force the DR output into negative saturation for forward current limit and positive saturation for reverse current limit.

The current reference will also program the CEMF output to a level proportional to the CFB level and the COMP adjustment.

The load instrument output IMET will also respond to the current reference.

The gain of the drive is reduced so that the phase control reference $P C R$ is equal to the magnitude of the driver reference $D R$ as long as the current reference is set to zero

With an oscilloscope, the initial pulse output IPU, and the pulse output PO may be montored to verify proper operation. See Figures 17 and 19.

## DIAGNOSTIC RUN (SWITCH RIGHT)

In diagnostic run, the local reference $L R$ and the diagnostic switch are substituted for the reference(s) SR, JOGR and the RUN and JOG switch inputs just as in diagnostic statıc. MA is inhibited from picking up in diagnostic run on Maxspeed Drives to prevent running beyond operating limit switches.

## CALIBRATION PROCEDURE

The diagnostic card is used to generate the appropriate test signals and operating modes to calibrate the drive. If a diagnostic card has not been furnıshed, one may be ordered or the test circuit shown in $\mathrm{F}_{\mathrm{I}}$. 22 may be used.

Make all connections prior to applying input power.
*All connections may be made to the test posts on the front of the main control card except for DFDR which is located on the 5TB terminal board.


DIAGNOSTIC STATIC

FIG. 22 DIAGNOSTIC TEST CIRCUIT
To avoid confusion and pussble meraction, the adjustments should be made in the following sequence The hosst and lower programming card adjuatments are necessary only when motor field programming in provided. Refer to the system elementary to determme what his heen furnished

TABLE IV Recalibrating Adjustment Sequence

|  | $\mathrm{MCC}, \mathrm{MFO}$ <br> AND IFC <br> ADJUSTMENTS | MDR ADJUSTMENTS |
| :---: | :---: | :---: |
| DIAGNOSTIC STATIC MODE, ADJUST |  | A LEVEL |
|  | FMAX | B LEVEL |
|  | FMIN* | 2ERO ADJ |
|  | floss | SFA |
|  | SLIM | MFH |
|  | cross* | HB |
|  | LIN TIME | MFL |
|  | COMP | SLI |
|  | CUR LIMIT | LB2 |
|  | IMET (IF | SL2 |
|  | USED) | LB3 |
|  | AIIGN | SL3 |
| DIAGNOSTIC <br> RUN MODE ADJUST | dIAGNOSTIC RUN MOIEIS INIIBITLED |  |
| NORMAL MODE, ADJUST | MAXSPEED |  |
|  | CEMF LIMIT | MAX NEG |
|  | REF SCALE | MAX POS |
|  |  | Slow |
|  | GAIN | (IF USED) |
|  | RESPONSE | MFH |
|  | DAMP | MFL |

*NOTE: 4 motor field control card is furmshed on base speed drives (comstant field) to provide field economy, voltage montor, and field current regulation. Set CROSS full CW and FMIN per test data sheet.

All of the high voltage mputs to the controller have been scaled down with the scale factors shown on the test data sheet. For example: On a 240 V motor voltage feedback VFB will be 5 volts when the armature voltage is 216 volts. If VFB is 3.2 volt 4 . then the armature voltage is $3.2 \times 216 / 5$ $=1.38$ volts. If armature voltage is 67 volts, VFB will be 67 x $5 / 216=1.55$ volts. All values have a tolerance of $\pm 10 \%$.

All readings can have a tolerance of $\pm 10 \%$.

Seleet Dragnostur static and set the CUR REF and LOC
REF to the center positions.

## FMAX (Maximum Field)

Set the LOC REF potentiometer for -1 volt at LR. Adjust FMAX untıl FC corresponds to maximum field FC on the test data sheet.

## FMIN (Minimum Field - Limit)

Set LOC REF potentiometer for -7 volts at LR. Adjust FMIN until FC corresponds to minimum field FC on the test data sheet.

## FLOSS (Field Loss - Fault)

Set the LOC REF to center position and reset the drive. Adjust FLOSS full CCW.

Monsor Fi: and moye the LOC REF potentiometer Rev untsl Fi: correcprond to the field lose value on the test data sheet. Slowly rotate FLOSS CW untul the "Ready to Run" light turns off andocating a drive fault. Reset the drive.

## SLIM (Overvoltage Fault)

Set the LOC REF to center position and reset the drive. Adjust SLIM full CW.

Monitor SFB and move the LOC REF potentiometer Fwd until SFB corresponds to the overspeed limit on the test data sheet. Slowly adjust SLJM CCW until the "Ready to Run" light turns off indicating a drive fault.

## CROSS (Crossover - Field) (For drives with field programming)

Set CROSS full CCW to enable field programming. CRS on the MFC card should also be jumpered to common.

## LIN TIME (Linear Time)

Monitor TR and set to zero with the LOCREF potentiometer. Rapidly turn the LOC REF full Fwd and measure the time for TR to ramp to 10 volts ( $\pm 10 \%$ ). Adjust LIN TIME until this tume corresponds to the test data sheet linear time.

## COMP (Compensation - IR)

COMP should be set full CCW. IR compensation is not used on voltage regulated drives.

## CUR LIMIT (Current Limit)

Set CUR LIMIT full CW Adjust the CUR REF potentiometer until CFB corresponds to the current limit level on the test data sheet. Monitor DR and turn CUR LIMIT CCW until DR just moves away from zero.

## IMET (Load Instrument Calibration) (If used)

Adjust the CUR REF until CFB corresponds to full load current. Verify that the optional load instrument reads full load. If not, remove power; adjust IMET and repeat.

## ALIGN (Tachometer Loss Align-Fault)

Set $A L / G N$ full CW for voltage regulated drives.

The following adjustments are located on printed circuit cards in the modification rack (MDR).

## A LEVEL / B LEVEL

(Sets drop out point of signal level detector relays SI.A and SLB. Refer to GEK-24946 for details).

Set COMP full CW. Adjust CUR REF until CEMF is .3 volts ( $5 \%$ CEMF). Adjust $A$ LEVEL until SLA drops out.

Adjust CUR REF until CEMF is at the desired level for brake setting. Normally 6 volts ( $10 \%$ ) for travel drives and 1.2 volts ( $20 \%$ ) for hoist drives. Adjust BLEVEL untıl SLB drops out. Return COMP full CCW and CUR REF to center.

## 2ERO ADJ (Reference Card)

(Used with induction masterswitches). With the masterswitch in the OFF position set ZERO ADJ for $0 \pm .1$ volt at DlS on the reference card.

The following adjustments are on the Hoist and Lower Programming cards in the modification rack. If motor field programming is not provided proceed with the normal run adjustments. Set all adjustments on the Hoist and Lower card.

## SFA (Stand by Field Adjust)

Adjust SFA until FC corresponds to standby FC on the test data sheet.

## MFH (Minimum Field Hoist)

Monitor LR and set to -5.6 volts with LOCREF. Set 0 volts at CFB with CUR REF. Adjust MFH until FC equals the minımum field hoist value of FC on the test data sheet.

## HB (Holst Breakpoint)

Adjust $A B$ until $H B$ on the horst card corresponds to the value on the test data.

## MFL (Minimum Field Lower)

Monitor LR and set at +56 volts with LOCREF. Set 0 volts at CFB with CUR REF. Adjust MFL until FC equals the mınimum field lower value of FC on the test data sheet

## SLI (Slope 1)

Set CFB at the value listed on the test data. Adjust $S / I$ unt 11 FC equals the value listed.

## LB2 (Lower Breakpolnt 2)

Adjust LB2 until LB2 on the lower card corresponds to the value on the test data.

## SL2 (Slope 2)

Set CFB at the value listed on the test data. Adjust SL2 untıl Fl: equal- the whe hested

## LB3 (Lower Breakpoint 3)

Adjust LB3 until LB3 on the lower card corresponds to the value on the test data.

## SL3 (Slope 3)

Set CFB at the value listed on the test data. Adjust SL3 untal FC equals the value listed

Return the Diagnostic Switch to Normal.

## MAX SPEED (Maximum Speed)

Set REF SCALE full CW. Montor the armature voltage from DA1 to DA2 Adjust the masterswitch until the motor is running at actual top voltage Adjust MAX SPEED until SFB is 10 volts.

## CEMF LIMIT (Counter EMF Limit)

Turn CEMF IIMIT full CCW and set the masterswitch at full throw. Adjust CEMF LIMIT until CEMF corresponds to the CEMF LIMITT on the test data sheet. Return REF SCALE full CCW.

## MAX NEGIMAX POS (Maximum Reference)

Move the masterswitch to the full hoist or forward position. Adjust the MAX NEG potentiometer until SFB is +10 volth. This normalizes the timed reference TR and system feedback, SFB for 10 volts at top voltage. Move the masterswitch to the full lower or reverse position. Adjust the MAX POS potentiometer until SFB is -10 volts.

## SLOW (Slowdown or Spotting Reterence)

With the masterswitch at full throw, artuate the thumb switch, spotting pushbutton or slowdown limit switch to drop out the slowdown relay. Adjust SLOW for the deared slowdown or spotting speed. Normally, SLOW in set at 20 $25 \%$ of maximum voltage.

## MFH and MFL (If used)

With the masterswitch at full throw, trim the MFH and MFL adjustments for the no load honting and lowermy top speeds.

## GAIN, RESPONSE, and OAMP (Stability Adjustments)

1 Set DAMP potentiometer at minimum 7 o'clock position.
2. Set the GAIN adjustment by calculating the GAIN number and referring to the chart (Fig. 23).

Gaın No $=$ Maxımum Operating Speed
Motor Base Speed

time - gain pot setting
Time-Gain Pot Setting
FIG. 23 GAIN ADJUSTMENT
After this setting has been made, make no further adjustments to the Gain Pot.

See motor nameplate under - Speed.
Motor Base Speed/Maximum Operating Speed.

Example: 1150/3600 RPM
3. Set LIN TIME potentiometer at minimum (7 o'clock).
4. Set RESPONSE potentiometer at mınımum ( 7 o'clock).

When the drive is functioning properly in all other respects make small incremental step increases and decreases in speed below base speed. Observe armature current for bumping repeatedly before steady state speed is attained.

Increase the RESPONSE setting (move CW) until bumpy current is observed. Then reduce the RESPONSE setting until no bumps (or only one) is observed. This is the maximum RESPONSE setting.

In general, settungs below $100^{\circ}$ clock will show signs
of increasing sluggishness. Settings greater than 2 o'clock may show signs of hard or even continuous bumping. Full RESPONSE setting (5 o'clock) will usually trip the IOC.
5. Reset LIN TIME to required setting.

## TROUBLESHOOTING

Although many of the problems which may arise can be effectively located with a multi-meter, an oscilloscope is a very powerful trouble shooting tool. The only requirements are that the selected scope have a $D C$ input capability and a line synchronzation mode. Caution should be exercised in measuring any point with a possible high potential with any instrument; however, particular care should be taken with an oscilloscope since the common clip is normally connected directly to the instrument case. If the grounded plug has not been defeated, it will cause a short crrcuit between the high potential point under test and ground.

## RECOMMENDED INSTRUMENTATION

Simpson Multi-meter (or equivalent) $10,000 \mathrm{ohms} /$ volt (or higher).

Hewlett-Packard, Tektronix or equivalent dual trace oscilloscope rated for operation from DC to 10 MHZ at $0.01 \mathrm{~V} / \mathrm{CM}$ with deflection factors to provide $0.01 \mathrm{~V} / \mathrm{CM}$ to 1300 peak to peak deflection when used with appropriate attentuator probes.

## PROCEDURES

In trouble shooting this drive system the most appropriate place to start is to follow the SFQUENCF OF OPERATION (previously described) untul a discrepancy or fault is noted. This step by step procedure will determine which part, subassembly or printed circuit card is causing the problem.

Included in this procedure is the use of the built-in Diagnostic Card (DGC) (or Test Circuit Fig. 22). This is another powerful tool for quickly locating drive system faults.

If the malfunction is a performance problem, then the quickest way to discover the problem is to follow the CALIBRATION PROCEDURE (previously described). There are two calibratıon procedures: (1) Without motor field programming (Maxspeed 100) and (2) With motor field programming (Maxspeed Hoist drives).

Detailed adjustments are found in GEK-24971 for the MFC card.

## HOW TO TEST AN SCR

## WARNING

ELECTRIC SHOCK CAN CAUSE PERSONAL INJURY OR LOSS OF LIFE. WHETHER THE AC SUPPLY IS GROUNDED OR NOT, HIGH VOLTAGES TO GROUND WILL BE PRESENT AT MANY POINTS THROUGHOUT THE SYSTEM.

1. Disconnect the AC power and make sure the loop contactor (MA) is open.
2. Using a multi-meter selected to read ohms on the time 1 K scale, check the forward and reverse resistance of each individual SCR cell. This is done by reading across power terminals T1 and DA1, T2 and DA1, T3 and DAl See conversion unit elementary diagram. Cood or faulty SCR's will give the following typical readıngs:

| SCR <br> Description | Forward <br> Reading | Reverse <br> Reading |
| :--- | :--- | :--- |
| Good SCR <br> Shorted SCR <br> Inoperative SCR <br> Open SCR | 100 K to Infinity <br> Zero <br> 1 to 2 K <br> 100 K to Infinity | 100 K to Infinıty <br> Zero <br> 100 K to Infinıty <br> 100 K to Infinity |

3. Since an open SCR will give about the same resistance reading as a good SCR, another method must be used to find this type of fault It should be pomted out; however, that practically all cells fall by hhorting and very few by opening If an open $S C R$ is suspected or it is desired to check the switching operation of an SCR, the following curcuit should be used:


FIG. 24 SCR TEST CIRCUIT

The multimeter is selected to read ohms on the 1 K scale, and is connected to read the forward resistance of the SCR. When switch $S W$ is closed, the forward resistance of a good SCR will change from a high value ( 100 K to mimity) to a low value (I to 10 K ). When the switch is opened a good SCR will revert to its high forward resistance or blocking state, if the holding current (multi-meter battery) source is momentarıly removed A faulty SCR will not switch remaning in either an open or a conducting state.
4. If any SCR's are suspected of being faulty from the above resistance checks, the appropriate SCR converston module should be removed from the case. After the SCR cathode and gate leads have been disconnected, recheck the forward and reverse resistances before replacing the SCR heat simk assembly This should be done before any SCR is definıtely classified as damaged or faulty, since a fault in another SCR or another part of the circuitry can produce a faulty reading from a good SCR before it is disconnected from the carcuit

## REMOVAL/REPAIR

## CONVERSION MODULE

The conversion module is best removed as follows. Disconnect the three AC input power and DC output leads.

(Photo Mif, 5236 ?
FIG. 25 REMOVAL OF GATE LEADS

Disconnect the SCR gate leads from the terminal board MTB. If markings are not legible. remark prıor to removal.

(Photo MG-5236-10)
fig. 26 REMOVAL OF SLOTtED SPACER
Loosen two nuts on the right hand side and remove the slotted spacer.

(Photo MG-5236-22)
FIG. 27 REMOVAL OF CONVERSION MODULE

Slide module to the right and pull out.

## SCR REPLACEMENT

The joint between the SCR and the heat sink performs two functions: (1) it carries the current and (2) it conducts the heat out of the SCR. To perform these functions properly, special care must be taken when reassembling an SCR to the heat sink as follows:

## STUD MOUNT SCR'S

Clean all surfaces of old lubricant and stray dust. Apply a thin film of General Electric G322L VERSILUBE ${ }^{\text {TM }}$ and tighten with a torque wrench to the following specifications:

STUD SIZE
$1 / 4 \cdot 28$
1/2-20

(Photo MG-5236-26)
FIG. 28 STUD MOUNT HEAT SINK (Front View)

(Photo MG-5236-27)
FIG. 29 STUD MOUNT HEAT SINK (Top View)

## PRESS PAK SCR'S

Clean both surfaces of old lubricant and dust. Apply a thin film of General Electric G322L VERSILUBE. Line up the assembly and evenly tighten the nuts finger tight. Tighten the nuts, one at a time, alternating between nuts according to the following specifications.

(Photo MG-5236-24)
FIG. 30 PRESS PAK HEAT SINK (Front View)

(Photo MG-5236-18)

## FANS (if supplied)

Remove the fan wires from the terminal board assembly and remove the two screws holding the terminal board assembly to the fan shelf. Loosen the two nuts on the bottom of the fan bracket and slide the fan bracket out.

(Photo MG-5230-23)
FIG. 32 REMOVAL OF FANS

## NOTE

There should be no need to retune the drive after removal/repair of a conversion module, an SCR or any other removable sub-assembly unless, of course, an adjustment was madvertently moved or disturbed. If a printed circuit card is replaced (other than the power supply card PSC):

1. Add stab-on jumpers to the replacement card just like the jumpers on the card that was replaced or as listed on the System Elementary Diagram "Programming" Table.
2. Add stab-on resistors and capacitors to the replacement card just like the components on the card that was replaced or as shown with values on the system elementary main control card (MCC) at stab-on terminals TR, RJ, SFB, NDE, CL1, CLJ, and LT2 or on the DM1, DM2, etc.
3. Set the potentiometers on the replacement printed crrcuit card to the position as was set on the card that was replaced or the position shown on the test data sheet. Recheck the recalibration procedures described.

FIG. 31 PRESS PAK HEAT SINK (Top Vlew)
4. Use caution when connecting or disconnecting stab-on connectors on the printed circuit cards to avord breaking of the connector posts. Support the card if possible and use a pair of long nosed pliers to hold on to the connector crimp. Avord pulling on wires when removing connectors.

## MODIFICATION FEATURES

With the varioun types of crane drive applications, there are many special features required which differ from one crane drive system to another. Below are histed some of the more frequently used features which may be found in a particular crane drive.

## LIMIT SWITCHES

There are varous functions of limit switches. An "operating" limit switch may bring the drive to a stop or slowdown the drive as part of normal operation. The stop is by regenerative braking before settung the brake, and the slowdown may simply recalibrate the regulator reference for a slow speed.

A "back-up" or "overtravel" limit switch is designed to imtrate an immediate stop by setting the brake and preconditıoning the drive. Such a limit switch may be an overhoist or end-of-travel limit switch.

A "power" limit switch is sometimes required as an overhoist limit switch which actually interrupts the power loop of the D-C motor and connects a dynamic braking recistor across the motor armature (Fig. 33). A contact on the power limit switch (PLS) deenergizes the brake directly. When backing out of the limit switch, the masterswitch picks up the lower contactor (L) which bypasses PLS energrzing the brake and applying power to the motor armature.


## STATIC EXCITER

The static exciter is a full-wave, single-phase bridge supplying constant-potential, direct-current power supply, employing static components. It consists of a transformer, rectifiers, and protective components. See GEI-43710. It provides DC control power for DC shoe brakes.

## EMERGENCY DYNAMIC BRAKING

This safety modification is designed to prevent the free fall of an overhauling load under the condition of simultaneous failure of the power supply and the holding brake. This is accomplished by a contactor which drops out due to loss of power, inserting a resistor across the motor armature. The voltage across this resistor is then fed through a rectifier bridge, for the correct polarity, to the motor shunt field to self-excite the motor for a controlled lowering speed.

## LOAD SPOTTING

The masterswitch is recalibrated to provide $25 \%$ speed at full throw. This reduces the mınimum hoisting \& lowerıng speeds and gives the operator more accurate speed control for spotting the load.

## LOAD FLOAT

The load float is to enable the operator to hold or spot the load without the use of the holding brake. Load float control is initiated by depressing the masterswitch thumb latch or a pushbutton which releases the brake and recalibrates the drive speed relationship. Top drive speed now becomes 20 to 25 percent of normal speed.

NOTE: The motor capability limits the time of stalling at absolute zero speed.

## TRANSFER SWITCHING

For some crane drive systems the same crane drive may be operated from different control locations, in which case it is necessary to transfer the crane drive control from one masterswitch to another. This transfer may be accomphshed by SB type switches or relays.

## RADIO REMOTE CONTROL

Radıo control can be substituted for the masterswitch for remote operation. By the nature of radıo control, all speed control is stcpped and all functions and interlocking must be performed by relays.

FIG. 33 POWER LIMIT SWITCH CIRCUIT

## PENDANT STATION

A pendant station may be substituted for the masterswitch for a floor-operated crane. On a pendant station, the speed potentiometer is operated by depressing the hoist or lower pushbutton proportional to the speed required. While a masterswitch can have twelve contacts (standard maximum) for interlocking, the interlocking must be performed by relays for a pendant station control. Other functions supplied in an operator's cab, such as a spotting pushbutton, are supplied on the pendant station.

## TRAVEL MOTIONS

Many crane drives require bridge, trolley, gantry, or a combination of motions to be incorporated in one crane drıve system. Depending on the application and duty cycle, the travel motions may be operated simultaneously with the horst, in which case separate drives are used for each function; or the travel motions may be operated with the hoist on a first-come, first-serve basis powered by the same drive. In this case, the hoist or travel motion is chosen by a selector switch or by whichever masterswitch is operated first, locking out the other functions.

Each travel motion then has the same protective devices, brake circuitry and provisions for limit switches as described previously for the hoist function. Two differences for travel motions are that (1) the torque or current limit function is normally set for 150 percent of rated torque, and (2) the drive is allowed to regenerate to 10 percent armature volts before setting the brake on a stop. These lower settings prevent skidding of wheels and make braking less severe.

## TRAVEL DRIFT

The travel drift modification is to enable the operator to "coast" the crane drive for a travel motion. Drift control is initiated by depressing the masterswitch thumb latch or pushbutton which releases the travel brake and recalibrates torque or current limit. The current hmit now becomes 50 percent instead of 150 percent of rated current, thus reducing the braking torque during the regeneration to a low value.

## HOIST MOTOR FIELD PROGRAMMER

(Refer to GEK-45130 and GEK-45131 for hoist and lower programming card elementary diagrams).

The purpose of the motor field programmer is to control motor field current as a function of armature current to obtain a constant horsepower characterıstic. From no load
to some small hook load, depending on the characteristic, the motor shunt field is held constant; from that point to approximately 100 percent rated hook load, armature current is constant and the field 15 varied to change speed and torque to give a constant horsepower characternstic. At 100 percent rated load, the motor field control reachen a maximum output, and the motor field is held ensentially constant for further increases in load

The motor field programmer consists of the motor held control, the hosst programming card (HPC) and the lower programming card (LPC).

In the OFF position, the field i, set by the field economy carcuit on the motor field rontrol, which reducen the field excitation to $70 \%$ of the SFA setting whenever the drive is shut down.

A direction sensing crecuit on the honst card sensen the polarity of the CEMF signal. When the CEMF signal in negative, pin 23 will switch positive to open a FliT swith and provide an off bias signal (KI) to the lower cad. When the CEMF agnal in positive, fun 23 will switeh negative to open another FET switch and provide an off bas signal $(\mathrm{KH})$ to the hoist card.

With zero volts at CFB and CEMF, the SFA potentiometer on the hoist card has an adjustment range of $75 \%$ by $100 \%$ of the nominal field current as set by FMAX on the MFC: card. This allows SFA to be set at the rated field level and FMAX to be set for a field forcmg level of up to $3.3^{\prime \prime}$ "

MAX. LOWER WEAK FIELD

MAX. HOIST WEAK FIELD


FIG. 34 MOTOR FIELD VERSUS ARMATURE CURRENT SIGNAL (Typical Curve)

## HOIST

In the hoist direction, a negative CEMF signal on pin 25 of the hoist card is inverted to provide a positive signal at pin 30. This signal weakens the motor field. The MFH adjustment adjusts the amount the field is weakened and therefore is used to set the no load hoist speed (Point A on Fig. 34). If the (FB signal, which is negative in hoisting, exceeds a preset bias level, the voltage at pin 6 will go negative to strengthen the fjeld as a function of armature current. Field strengthening (Point B in Fig. 34) can be adjusted to occur from $80 \%$ to $100 \%$ of rated current by hoist bias potentiometer $\mathcal{H B}$.

The gain of the field strengthening circuit (Slope C, Fig. 34) may be decreased by connecting pin 5 to pin 6 . It may be increased by connecting pin 5 to common.

During regenerative hoist operation, when CFB is positive, a bias signal is applied to OA2-2 to prevent field strengthening.

## LOWER

Positive CEMF in the lower direction will cause LV to go
positive and weaken the motor field. The MFL adjustment on the hoist card is used to set the no load lower speed (Point lon Fig. 34).

The field increase as a function of 2 CFB is controlled by three amplifier stages. The first stage (OA2-1) increases the field current with no offset bias. The gain (Slope 1 on Fig. 34) is adjusted by SLI. The second stage (OA3-1) is biased such that additional field increase starts at a given armature current (Point 2 on Fig. 34). This bias is set by potentiometer LB2. The gain (Slope 2 on Fig. 34) is set by SL2. LB3 sets the bias for the third stage amplifier, OA3-2 (Point 3 on Fig. 34). SL3 sets the gain of OA3-2 (Slope 3 on Fig. 34).

The adjustments for the lower characteristic must be made in the sequence as listed in the Calibration Procedure.

Output filtering on both the voltage and current programming sections of the lower card controls the rate of change of the motor field. The time constants of OA1-2 and

0A4－2 may be changed by jumpers connected from pins 3 and 30 ．The time constant in the voltage section may be increased by moving the jumper from pin 18 to pin 21,24 or 25 ．The time constant in the current section may be increased by moving the jumper from pin 10 to pin 7,8 ，or 6.

Increasing these constants will decrease the amount of speed overshoot when lowering full load but will also increase the lower no load acceleration time to top speed．

The motor field may be set up in the＂Diagnostic Static＂ mode．The CEMF signal is replaced by FDR（Field Diagnostic Reference）which is changed with the LOC REF potentiometer on the diagnostic card．The CUR REF potentiometer allows for varying the CFB signal to program the field．

In the＂Diagnostic Run＂mode－ 20 V is applied from DGC （MAC）to DMAC on pin 29 of the lower card and pin 3 of the hoist card．This signal closes FET switch T2，applying diagnostic reference LR to the MFC（FDR）and inhibits the hoist card output CRM．This allows the FMIN and FLOSS values to be checked．

## REFERENCE CARD（REF）

（Refer to GEK－45129 for the reference card elementary diagram）．

The reference card provides a circuit to convert the output of an induction masterswitch to a bidirectional DC reference for a reversing drive．With the induction switch connected to pins 8X，9， 8 and 6 the output（DIS）at pin 10 will vary from $-20 \mathrm{~V} \pm 2 \mathrm{~V}$ to $+20 \mathrm{~V} \pm 2 \mathrm{~V}$ for full throw of the masterswitch．

A reference polarity check is also provided．A negative input at pin 19X can be supplied to pin 30 or 30 X only if +30 V is applied to pin 11 （NSW）．A positive input at pin 19X can be supplied to pin 5 X or 3 X only if +30 V is applied to pin 13 （PSW）．

The voltage monitor circuit will generate a fault trip signal at SYS when a $25 \%$ error exists between the driver reference $D R$ and the system feedback SFB．When the voltage at pin 28 X exceeds 10 V the output of the latch circuit on pin 23 （SYS）will exceed +10 V to initiate a system trip．The OCK indicating light will also turn on．With the error voltage at pin 28 X reduced to less than 10 V ，the circuit can be reset with the reset pushbutton．

This circuit will also indicate an overvoltage fault（TF）as detected by the overspeed circuit of the MFC．

## TORQUE PROVING CARD（TQP）

（Refer to GEK－45128 for the torque proving card elementary diagram）．

The basic card function is to prevent releasing the motor brake until proper current response to both a positive and negative reference has been detected．

## SEQUENCE OF OPERATION

When preconditioning is released and a reference signal is applied，the TR voltage will time up as a function of the reference signal until the clamp level of 1.6 V to 2.0 V is reached．

The TR voltage is now inverted by OAl such that ATR＝ －TR．This ATR signal is applied to the regulator in addition to the TR signal，but at twice the current level resulting in a net effect of inverting the applied reference．

The initial test involves check for proper current polarity in response to the inverted reference．

For a negative input the TR voltage is negative and the ATR voltage is positive which should result in a positive C．FB signal．If $\mathrm{CFB}>+.8 \mathrm{~V}$ with $\mathrm{ATR}>+.8 \mathrm{~V}$ the voltage at pin 27 is pulled low（ $<1 \mathrm{~V}$ ），the voltage at pin 13 swings high $(>+15)$ and the voltage at ICI（4）swings low（ $<\mathrm{IV}$ ）tolateh in the circuit．When ICl（4）swings low，LEI）I（IC）is illuminated to indicate the detection of a positive CFB signal with ATR positive．

The second test is then initiated by checking for a curremt response to the TR reference only．As IC．1（4）swings low， transistor T8 is turned on to close the FET＇switches＇T6 and T7．This changes OAI to a non－inverting amplifier such that ATR＝TR．The auxiliary timed reference is now removed from the regulator by the closing of＇T＇7．The regulator then only sees the clamped TR voltage which should result in a current reversal．

For a negative reference as described above，both TR and ATR is negative and a negative CFB vollage should result． Thus，if $\mathrm{CFB}<-.7 \mathrm{~V}$ with ATR $<-.7 \mathrm{~V}$ the voltage at $\mathrm{p}^{\text {in }}$ 12 is pulled low，pin 10 swings high and the voltage at ICl（8）swings low to latch in the circuit．Now as IC．I（8） swings low LED2（HC）is illuminated to indicate the： detection of a negative CFB signal with ATR negative．

If the input reference is positive the test would be performed in the reverse order by LED2（H1C）being

## Illummated before LED I (LC)

With both current polarities detected, pin 10 and pin 13 have both changed to a high state $(>+15 \mathrm{~V})$ making $\operatorname{ICl}(10)$ swing low. The output of the second half of OA1 at pin 22 then switches from positive saturation to negatıve saturation. This turns on transistor T17 to energize the external BPR relay. At the same time T 2 is opened to remove the TR clamp, but now the Tl switch is closed for a pertod adjustable by Pl from zero to .5 seconds to clamp the TR voltage at zero until the brake opens.

If the imput signal in removed shortly after application, it is possible to detect and latch up in one direction, but not in the other as the reference 15 removed. If the test is not completed, t.e., if the voltage at pin 22 does not swing negative within 1 second following the detection of one current polarity transistor Tl6 will turn on to reset the circuit.

When the drive is preconditioned by the PRE voltage changing from -3.5V to zero, transistor Tl4 turns on to reset the circuit. In the Diagnostic mode a positive signal, DP'2, is applied at pin 6 to override the preconditioning reset which allows a diagnostic check of the circuit.

## TORQUE PROVING CHECK (TQP)

(A) Switch the Diagnotic Switch to static.
(B) Turn the LOC REF pot CW (+LR).
(C) Quickly turn the CUR REF pot CW, then CCW. Both lights on the torque proving card should light (HC first, then IC) and BPR should pick up.
(I) 'To renet T(OP', return the Diagnostic Switch to Normal, then bach to static.
(E) Turn the LOC REF pot CCW (-LR).
(F) Quickly turn the CUR REF pot CCW, then CW. Both lights should come on (LC first, then HC) and BPR should prek up.

## GLOSSARY OF TERMS

PAGE
ALIGN - Tachometer Loss Align Adjustment ..... 32
BPR - Brake Permissive Relay ..... 14, 22
*CEMF - Counter EMF ..... $26,28,30,32,39,40$
CEMF LIMIT - Counter EMF Limit Adjustment ..... $14,26,31,33$
*CFB - Current Feedback ..... $26,27,31,32,33$
*COM - Regulator Common ..... 21
COMP - IR Compensation Adjustment ..... 1, 30, 31, 32
CPT - Control Power Transformer ..... 14. 26
CROSS - Crossover Adjustment ..... 32
CUR REF - Diagnostic Current Reference Potentiometer ..... $24,32,33,11$
CUR LIMITT - Current Limit Adjustment ..... $11,26,31,32$
DAl - Positıve Armature Connection ..... 33
DAMP - Dampening Adjustment ..... 14, 30, 34
Diagnostic - Normal ..... 23, 33
Diagnostic - Run ..... 31
Diagnostic - Static ..... 30,32
DGC - Diagnostic Card ..... 14, 18, 34
*DM1 - DM8 Dummy Input/Output points
*DR - Driver Reference ..... $26,30,31,32$
*EAO - Error Amplifier Output ..... 26
EST - External Fault Stop ..... 21
F1 - F'2 - Motor Field Connections
*FC - Field Current Signal ..... 23, 33
FDR - Field Diagnostic Reference (DFDR) ..... 32
FEA - Field Economy Adjust
24
FF - Field Fault
FLOSS - Field Loss Adjustment ..... 32, 41
FLT - Fault Relay ..... 17, 20, 21, 24, 26
FMAX - Motor Field Maxımum Adjustment ..... 32, 39
FMIN - Motor Field Minımum Adjustment ..... 32, 41
GAIN - Speed Loop Gain Adjustment ..... $14,26,34$
HB - Horst Breakpoint Adjustment ..... 33, 40
HPC - Hoist Programming Card ..... $14,33,39$
IFC - Interface Card ..... $11,17,20$
IMET - Current (Load) Instrument Output and Adjustment ..... 17, 22, 31, 32
IOC - Instantaneous Over Current ..... 24
*IPU - Initial Pulse ..... 28, 30
*JOG - Jog Switch Input ..... 21,30
*JOGR - Jog Reference ..... 3)
L.B - Lower Breakpont Adjustment ..... 33
LIN TIME - Linear Timıng Adjustment ..... $14,26,30,32,34$

## GLOSSARY OF TERMS

## (continued)

PAGE
LOC: REF - Diagnostic Local Reference Potentiometer $24,30,32,33,41$
LPC - Lower Programmıng Card ..... $14,33,39$
*IR - Local Reference from DCC ..... 30, 31, 32, 33
MA - Line Contactor ..... $14,20,26,30$
*MAC - MAX Control Signal ..... 26
MAX - Pitot Relay for M ..... $17,20,21,26,30$
MAX NEG; - Maxımum Negative Reference Adjustment ..... 26, 33
MAX POS - Maxımum Positive Reference Adjustment ..... 26, 33
MAX SPEED - Adjustment ..... $14,26,33$
MCC - Main Control Card ..... $14,16,20$
MDR - Modification Rack ..... 19,20
MFC: - Motor Field Control Card ..... $14,18,20,31$
MFH - Minmum Field Hoist Adjustment ..... 23,33
MF'L - Minmum Field Lower Adjustment ..... 23, 33, 40
MIN SPEED - Adjustment ..... 14,22
MOV - Metal ()xıde Varistor ..... 19, 20
*OSC - Osellator ..... 24,28
*PCR - Phase Control Reference ..... 30, 31
PO - Pulse Outputs ..... $28,29,30$
*PRE - Preconditıoning ..... 26,30
PSC: - Power Supply Card ..... $14,18,20$
REF - Reference Card ..... 14, 41
REF SCALE - Adjustment ..... 14, 30, 33
RESPONSE - Speed Loop Response Adjustment ..... 14, 26, 34
RESET - Pushbutton ..... 21, 24
RSTOP - Regeneratıve Stop Adjustment ..... 17, 24
*RTR - "Ready to Run" Indicator ..... 21
*RUN - Run Switch Input ..... $21,22,26,30$
$\mathrm{Sc}: \mathrm{R}$ - Power Conversion Module ..... $14,20,26$
*SA, SB, SC - Synchromzing Signals ..... 26, 28
SFA - Standby Pield Adjustment ..... 33, 39
*SFB - Speed Feedback ..... $18,26,30,31,32$
Sl. - Slope Adjustment ..... 33
SLIM - Speed Limit Adjustment ..... 32
SLOW - Slow Speed Adjustment ..... 33
*SMET - Speed Instrument Output and Adjustment ..... 17, 22
*SMIN Minimum Speed Reference Adjustment and Input ..... 22
*SR - Spced Reference ..... $22,26,30$
*SYS - System Fault Trup ..... 24

## GLOSSARY OF TERMS

## (continued)

PAGE
*TA - Tachometer Align Output
TF - Tach Fault ..... 24
*TFB - Tachometer Feedback Signal ..... 30
TKN - Negalive Tachometer Input ..... 22
TKP - Positive Tachometer Input ..... 22
TQP - Torque Proving Card ..... 14, 42
*TR - Timed Reference ..... 26, 30
*VFB — Voltage Feedback ..... $26,27,30$
*WFR - Weak Field Reference ..... 26
XO - Isolation Transformer Secondary Neutral ..... 14
XO - Negatıve Armature Connection ..... 14
(1) Also see Motor Field Control Instructions, GEK-24971*TEST Points Located on Door Front (See MCC Illustrations, Fig. 6)

## HOT LINE TELEPHONE NUMBER

The Contract Warranty for MAXSPEED drives is stated in General Electric Apparatus Handbook Section 105, Page 71.

The purpose of the following is to provide specific instructions to the Maxspeed-Drive user regarding warranty administration and how to obtain assistance on out-of-warranty failures.

1. In the event of failure or misoperation during "in warranty" refer to the instruction book to identify the defective part or subassembly.
2. When the defective part has been identified (or for assistance in identification) call:

General Electric Company
Erie, Pennsylvania
814-455-3219
(24. Hour Phone Service)
or

Contact the nearest

General Electric Installation and Service Engineering Office listed in your telephone directory. Before calling, list model and serial numbers of the power unit and DC motor.

# GENERAL ELECTRIC COMPANY - DIRECT CURRENT MOTOR \& GENERATOR DEPARTMENT ERIE, PENNSYLVANIA 16531 


[^0]:    These unstructions do not purport to cover all detalls or variations in equipment nor to provide for every possible contingency to be met in connection with installation, operation or maintenance. Should further information be desired or should partucular problems arise which are not covered suffictently for the purchaser's purposes, the matter should be referred to General Electric Cumpany

